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ARMY MISSILE RESEARCH AND DEVELOPMENT COMMAND REDSTO--ETC F/G 20/4
USER'S MANUAL FOR THE MARTIN-MARIETTA HIGH ANGLE OF ATTACK AERO--ETC(U)
JUN 78 G C WINN

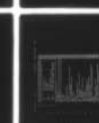
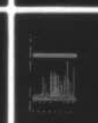
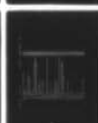
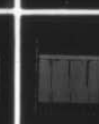
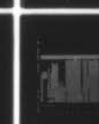
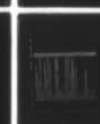
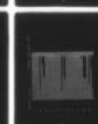
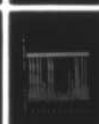
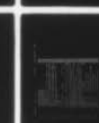
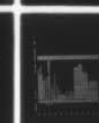
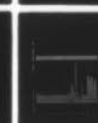
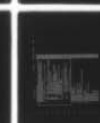
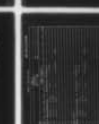
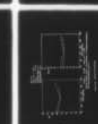
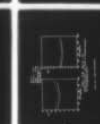
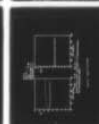
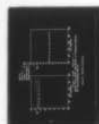
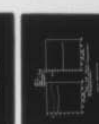
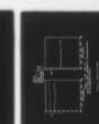
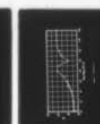
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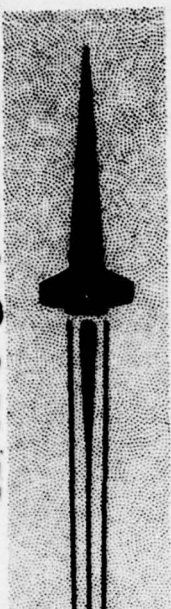
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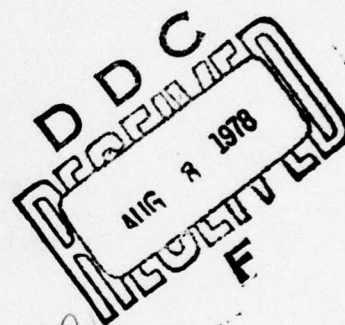


TECHNICAL REPORT T-78-63

**USER'S MANUAL FOR THE MARTIN-MARIETTA
HIGH ANGLE OF ATTACK AERODYNAMIC
METHODOLOGY FOR BODY-TAIL MISSILES**

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Aeroballistics Directorate
Technology Laboratory

JUNE 1978



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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report documents the computer program developed by the Army to evaluate and implement an aerodynamic methodology developed by the Martin Marietta Corporation. The methodology was developed to predict aerodynamic forces on slender missile bodies with low aspect ratio tails at low and high angles of attack, at arbitrary roll angles for both transonic and supersonic velocities.		

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I. INTRODUCTION

The Martin Marietta Corporation, Orlando Division, has developed an aerodynamic methodology and published a report (Ref. 1) under Contract No. DAAH01-74-C-0621 with the US Army. The report describes the development and application of semiempirical methods for predicting aerodynamic characteristics of slender body and body-tail configurations.

In an effort to evaluate the Martin Methodology, a computer program was developed to incorporate the various theoretical and empirical procedures called for in the Martin report. The results of this evaluation are covered in detail in Ref. 2. As a follow-up to the Martin Methodology analysis, a few modifications of the methodology were accomplished in an attempt to correct certain disagreements found between measured experimental data and associated predictions derived from the methodology.

This report is intended to be a user's guide for the use of the methodology program. The methods and procedures used in developing the aerodynamic methodology are covered extensively in Ref. 1 and only those modifications to the methodology implemented by the Army will be discussed in this report.

II. PROGRAM CAPABILITIES

The Aerodynamic Methodology Program can predict aerodynamic characteristics of slender body and body-tail missile configurations, to include the following predictions:

- 1) Body alone normal force, center of pressure, and axial force.
- 2) Isolated tail panel normal force and center of pressure.
- 3) Mutual interference effects that enable the prediction of normal force and center of pressure of body-tail combinations.

The program in its present form was developed to predict these characteristics for missiles with four fins in cruciform configuration, with the fin trailing edges flush with the missile body base. The fin numbering convention, as well as the conventions for angle of attack (α) and roll angle (ϕ), are shown in Figure 1.

The range of input parameters for the program are:

- | | |
|-------------------------------------|---|
| 1) Mach number | 0.8 to 3.0 |
| 2) Angle of attack | 0 to 180 for isolated components
(roll angle = 0). 0 to 45 for
body-tail combinations at arbitrary
roll angles from 0 to 180 . |
| 3) Tail leading edge
sweep angle | 0 to 70 degrees |

- | | |
|------------------------------------|---|
| 4) After-body length
(calibers) | 6 to 18 |
| 5) Nose length
(calibers) | 1.5 to 3.5 |
| 6) Tail taper ratio | 0 to 1 |
| 7) Tail aspect ratio | .5 to 2.0 (aspect ratio of two
tail panels joined at root chord) |

III. DISCUSSION

Certain modifications of the original methodology were incorporated into the methodology computer program. These modifications were an attempt to correct certain disagreements between experimentally obtained data and associated predictions from the methodology which became apparent during an evaluation of the **original methodology** (Ref. 2).

The modifications are limited to the body alone normal force prediction methods and involve the addition of newly obtained unpublished data. Specifically, equation 16, page 36 as depicted in Figure 20 of Ref. 1, has been eliminated and replaced by values of η (correlation factor for end effects) as shown in Figure 2 of this report. In addition, the crossflow drag coefficient versus crossflow Mach number curve shown in Figure 22a of Ref. 1, has been replaced by Figure 3 of this report.

Comparisons of predictions generated from the original methodology and those with the above modifications, compared with the experimental data, are shown in Figures 4 through 10 of this report.

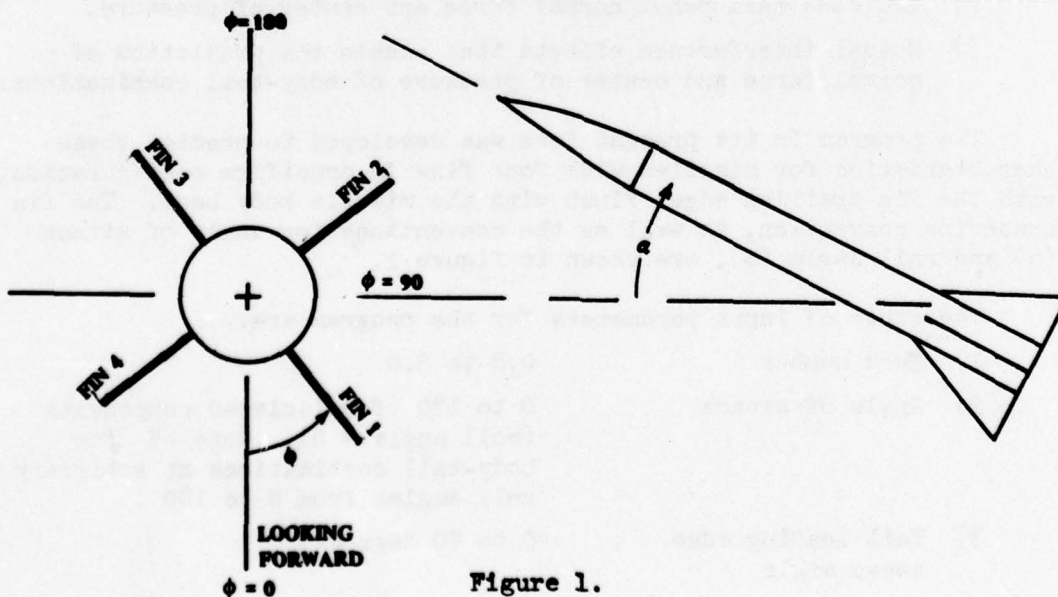


Figure 1.

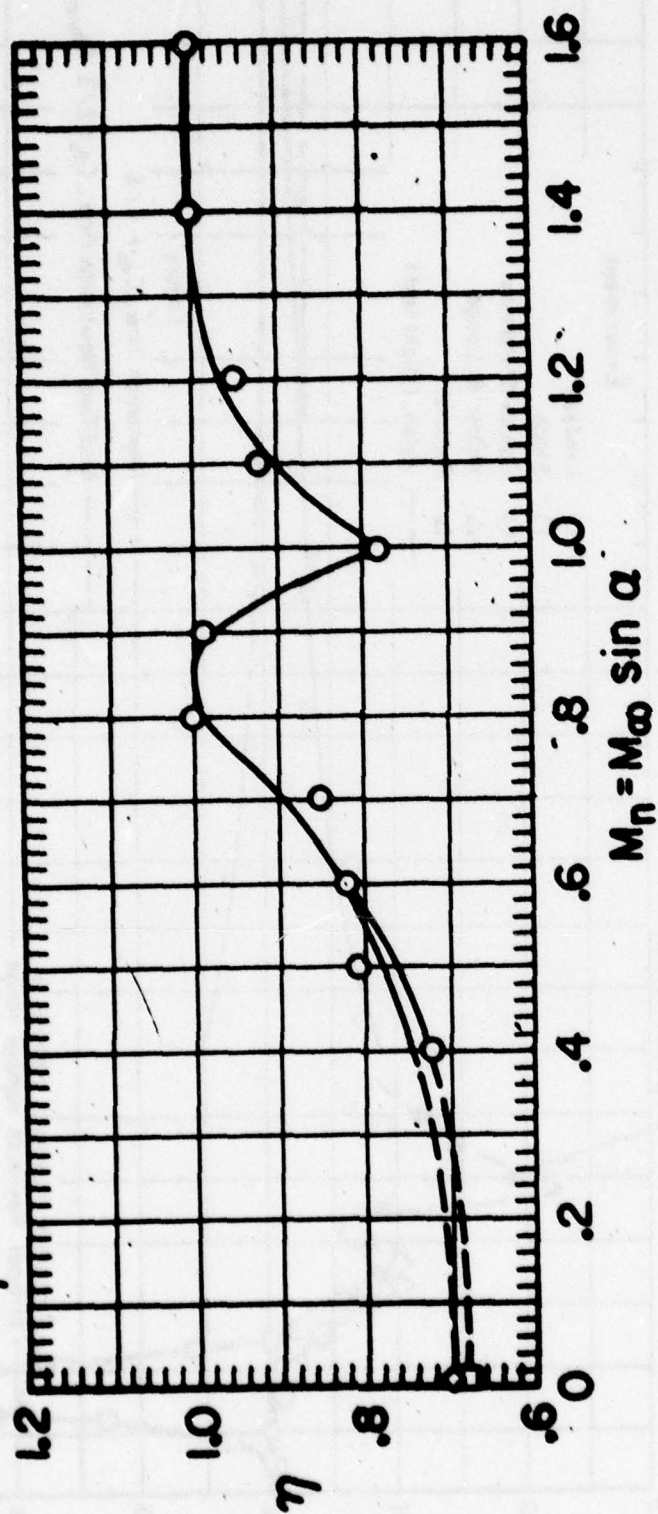


Figure 2. Values of η .

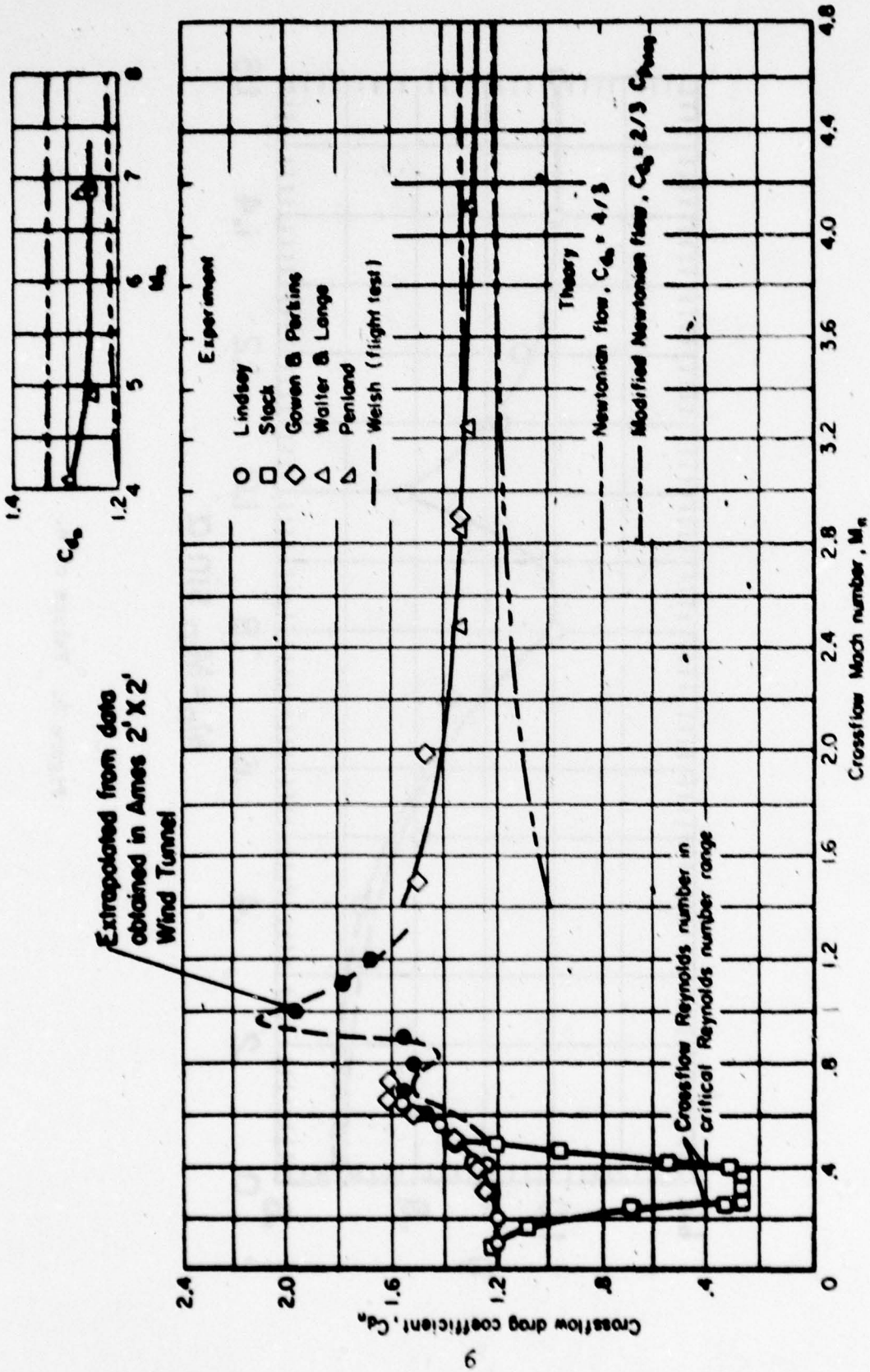


Figure 3. Unpublished data.

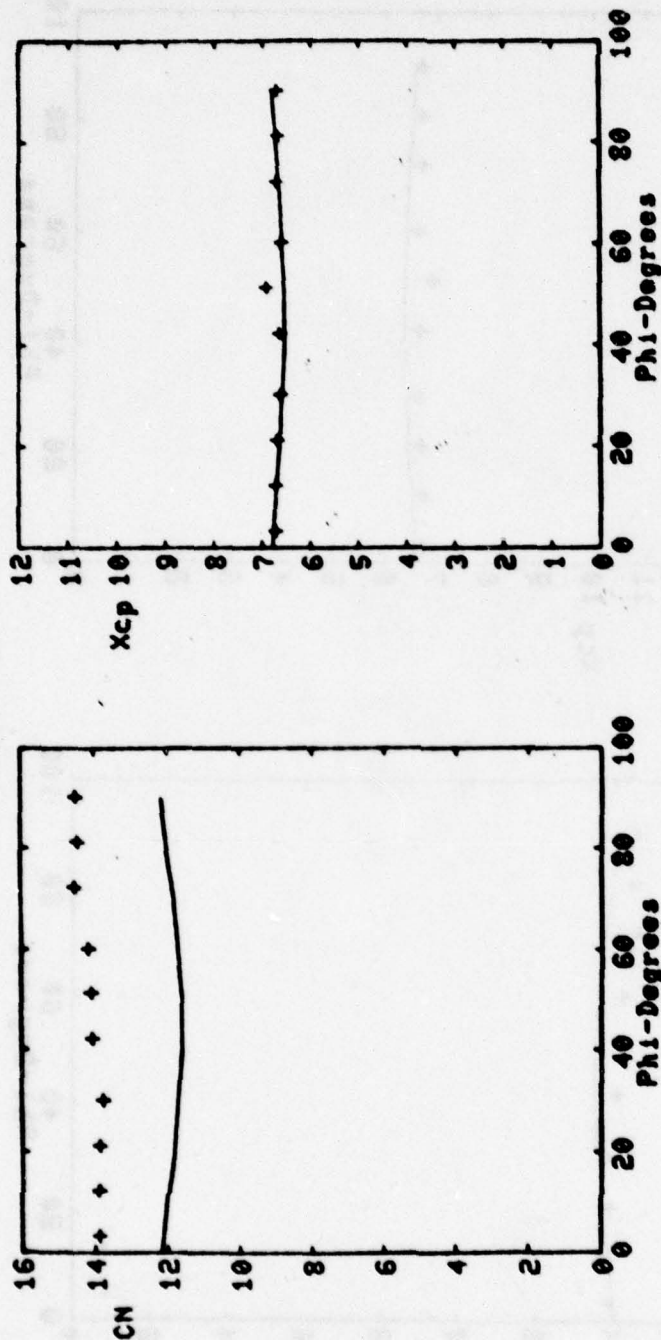
B3T1-5

Mach No = 1

Alpha = 44.92

Methodology--(-)

Experiment---(+)



Alpha = 44.92 Mach No = 1

Normal Force Coeff. And Center of Pressure Location
For Configuration B3T1-5

Figure 4a. Original methodology.

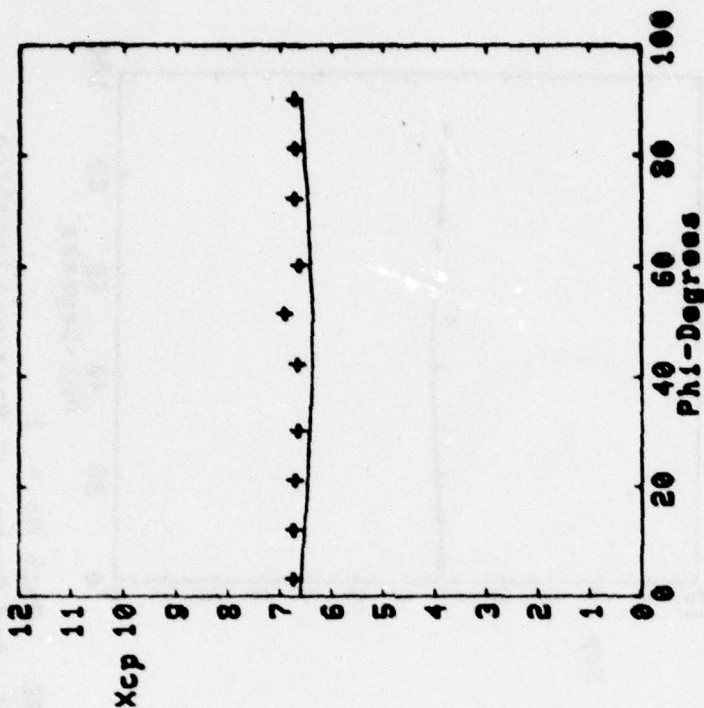
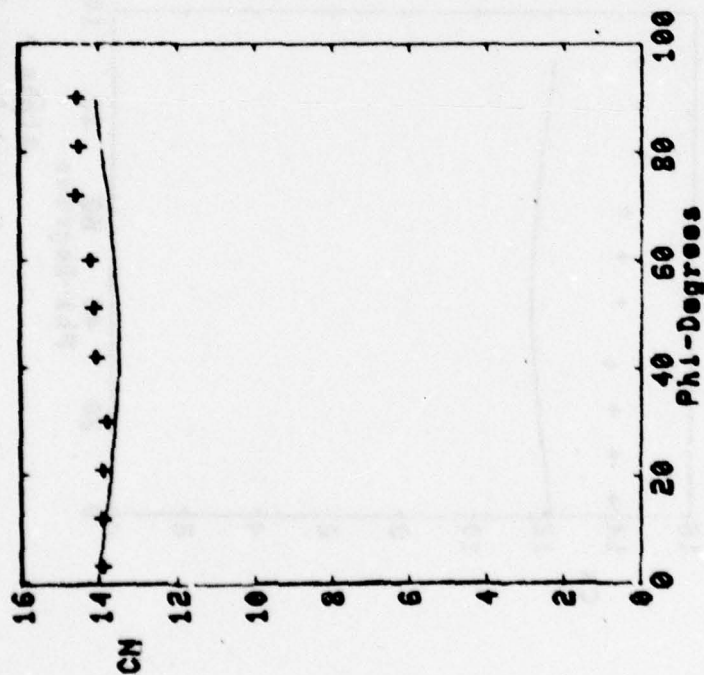
B3T1-5

Mach No. = 1

Alpha = 44.92

Methodology--(-)

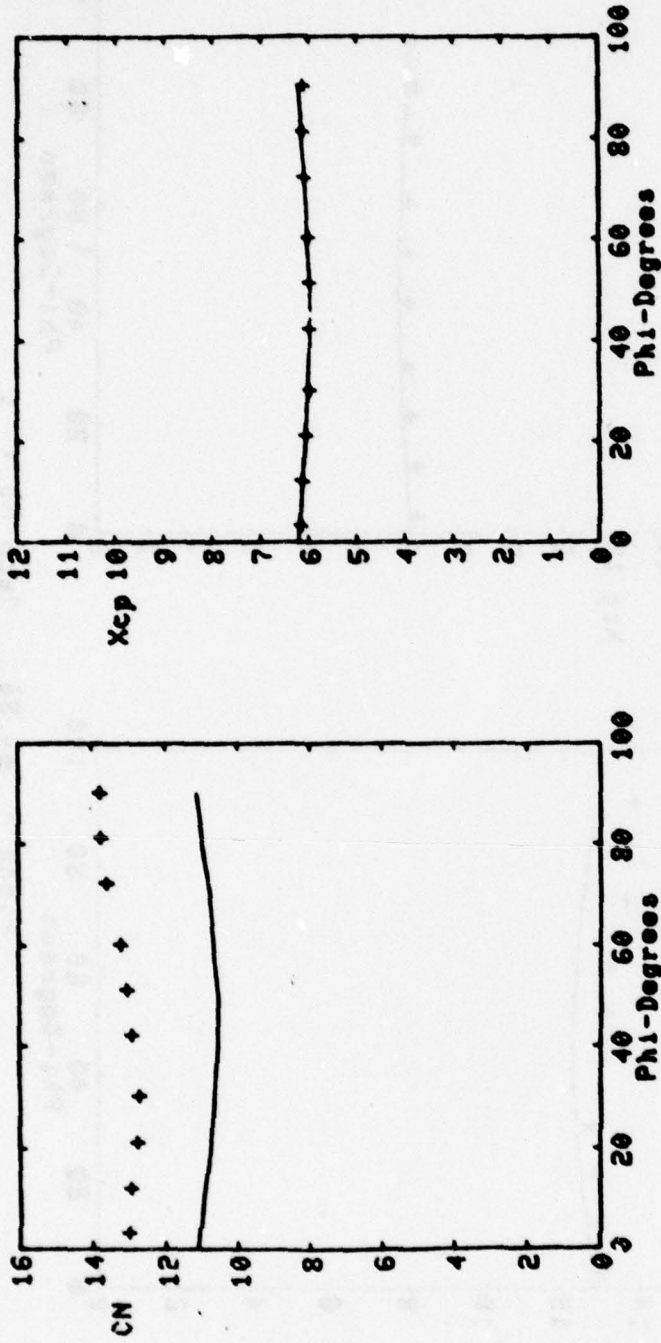
Experiment---(+)



Alpha = 44.92 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B3T1-5

Figure 4b. Modified methodology.

B2T1-5
Mach No. = 1
Alpha = 44.88
Methodology--(-)
Experiment---(+)



Alpha = 44.88 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B2T1-5

Figure 5a. Original methodology.

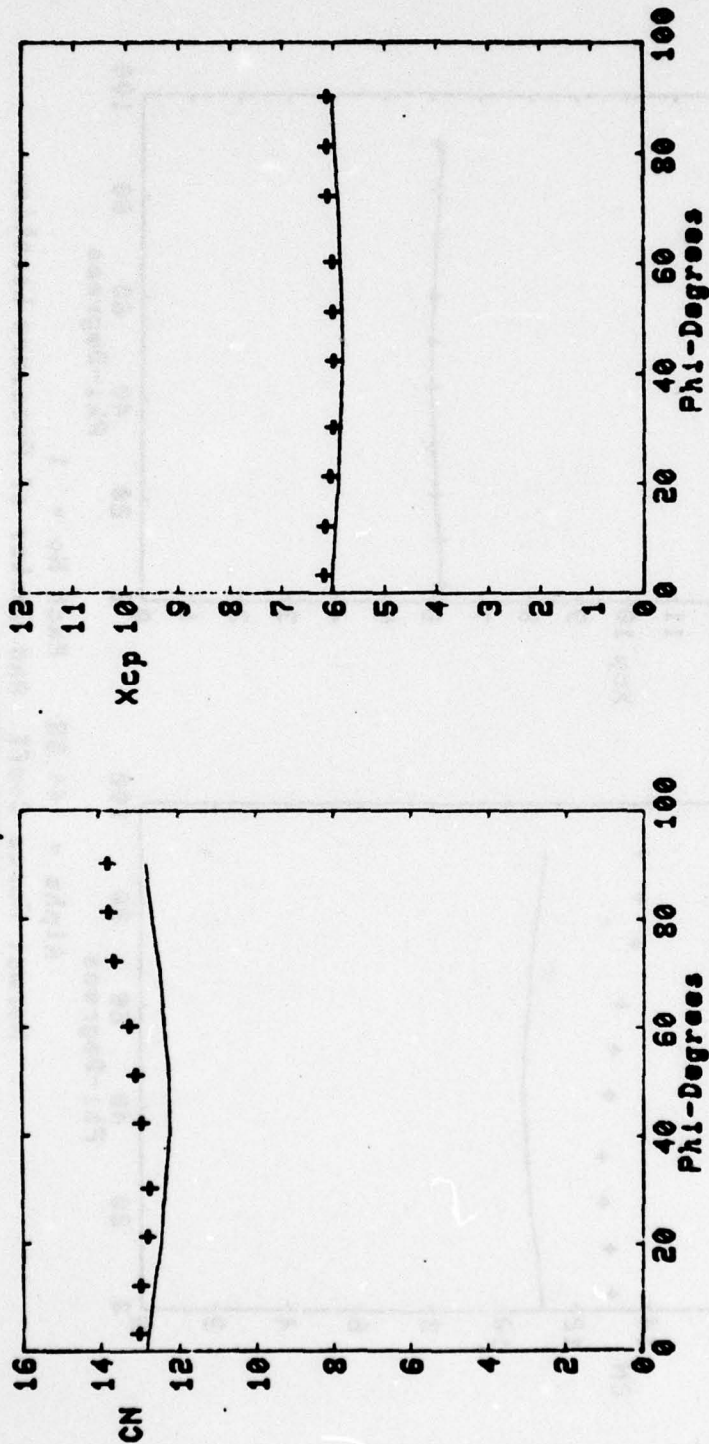
B2T1-5

Mach No. = 1

Alpha = 44.88

Methodology--(-)

Experiment---(+)



Alpha = 44.88 Mach No. = 1

Normal Force Coeff. And Center of Pressure Location

For Configuration B2T1-5

Figure 5b. Modified methodology.

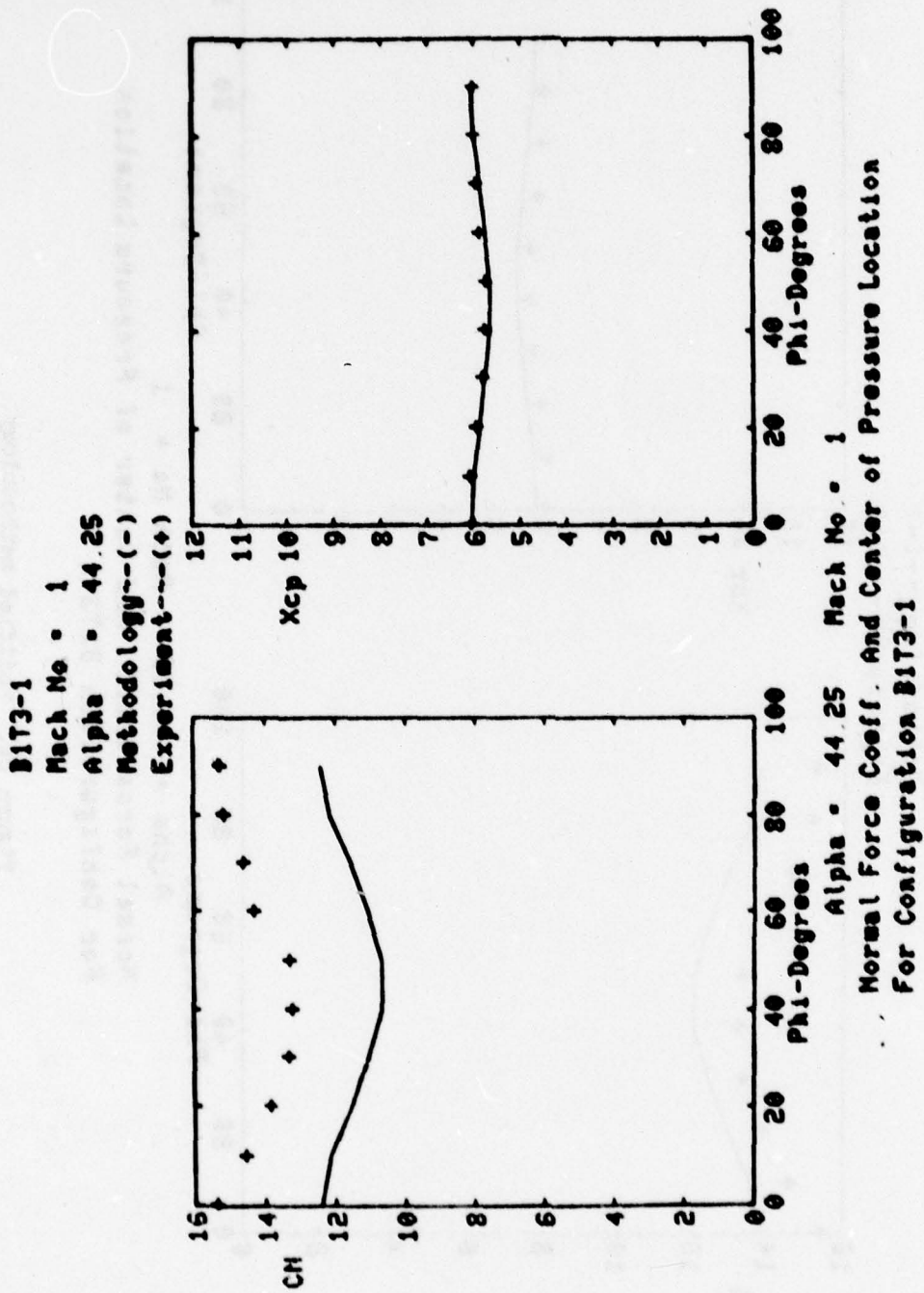
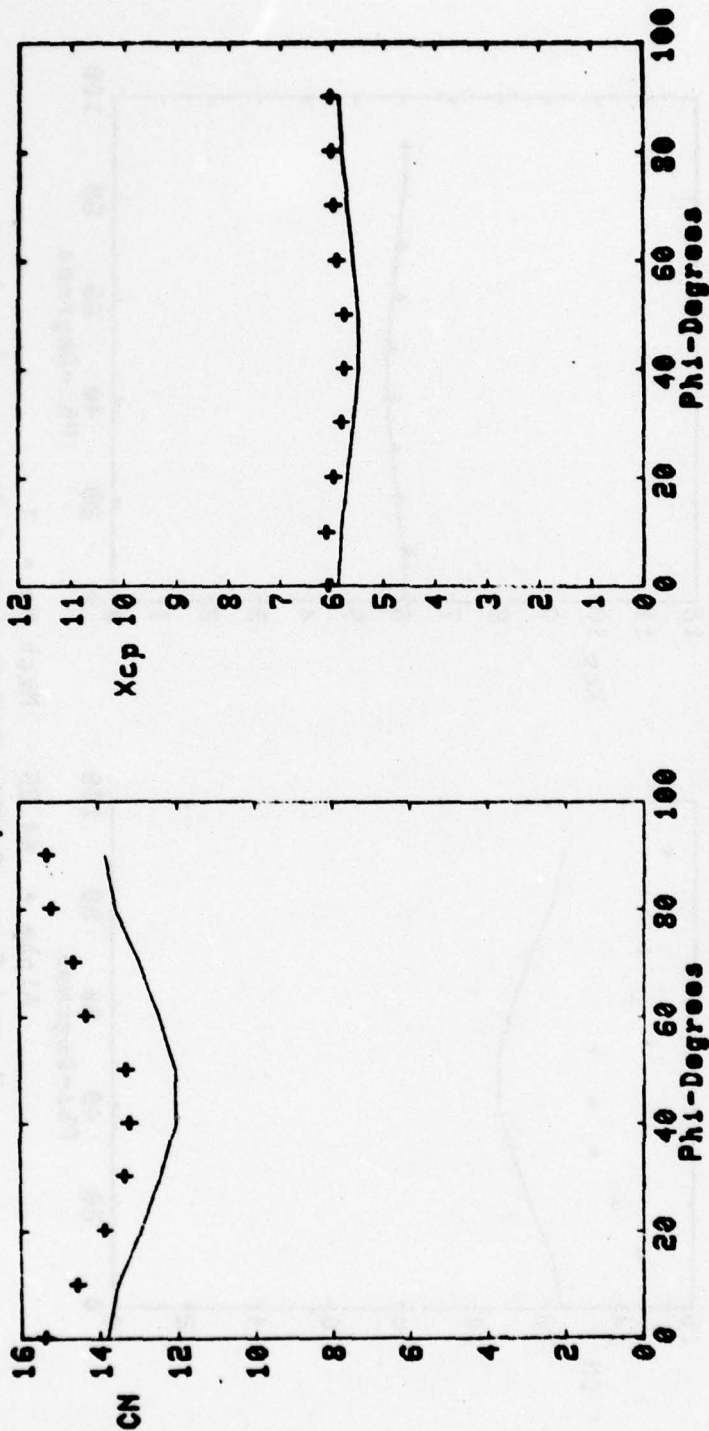


Figure 6a. Original methodology.

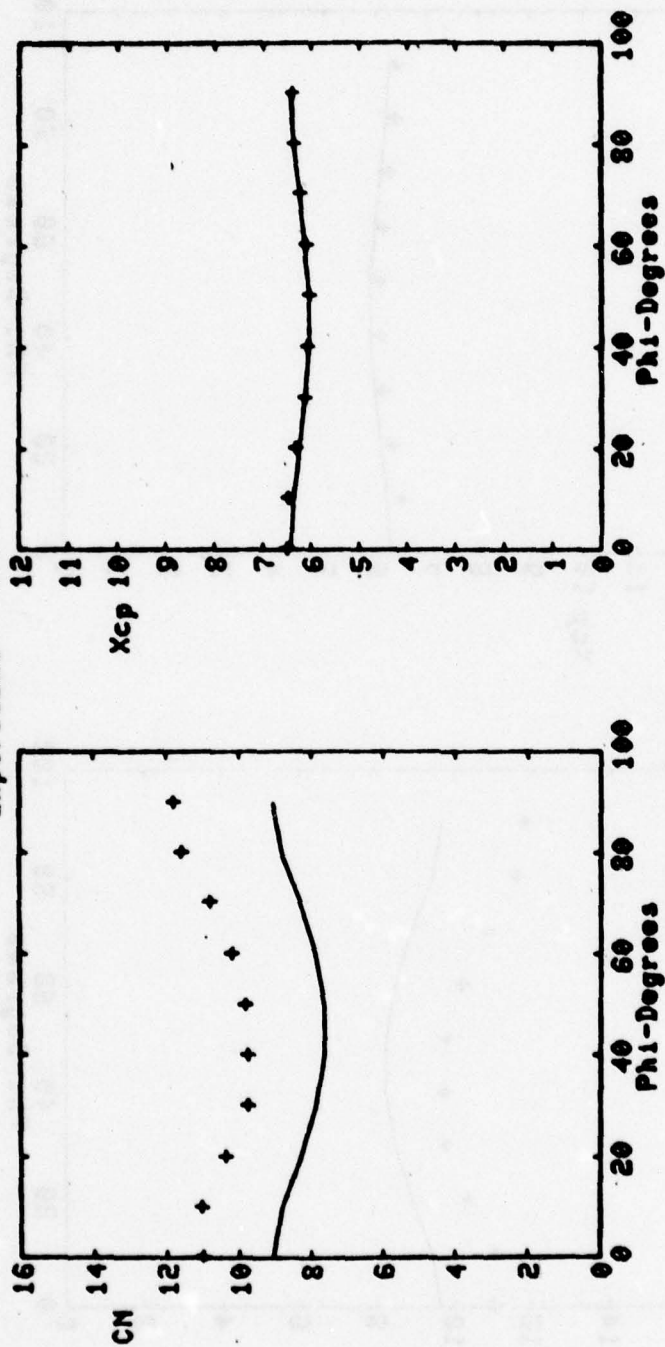
B1T3-1
Mach No. = 1
Alpha = 44.25
Methodology--(-)
Experiment---(+)



Alpha = 44.25 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T3-1

Figure 6b. Modified methodology.

BIT3-1
 Mach No. = 1
 Alpha = 34.95
 Methodology--(-)
 Experiment---(+)



Alpha = 34.95 Mach No. = 1
 Normal Force Coeff. And Center of Pressure Location
 For Configuration BIT3-1

Figure 7a. Original methodology.

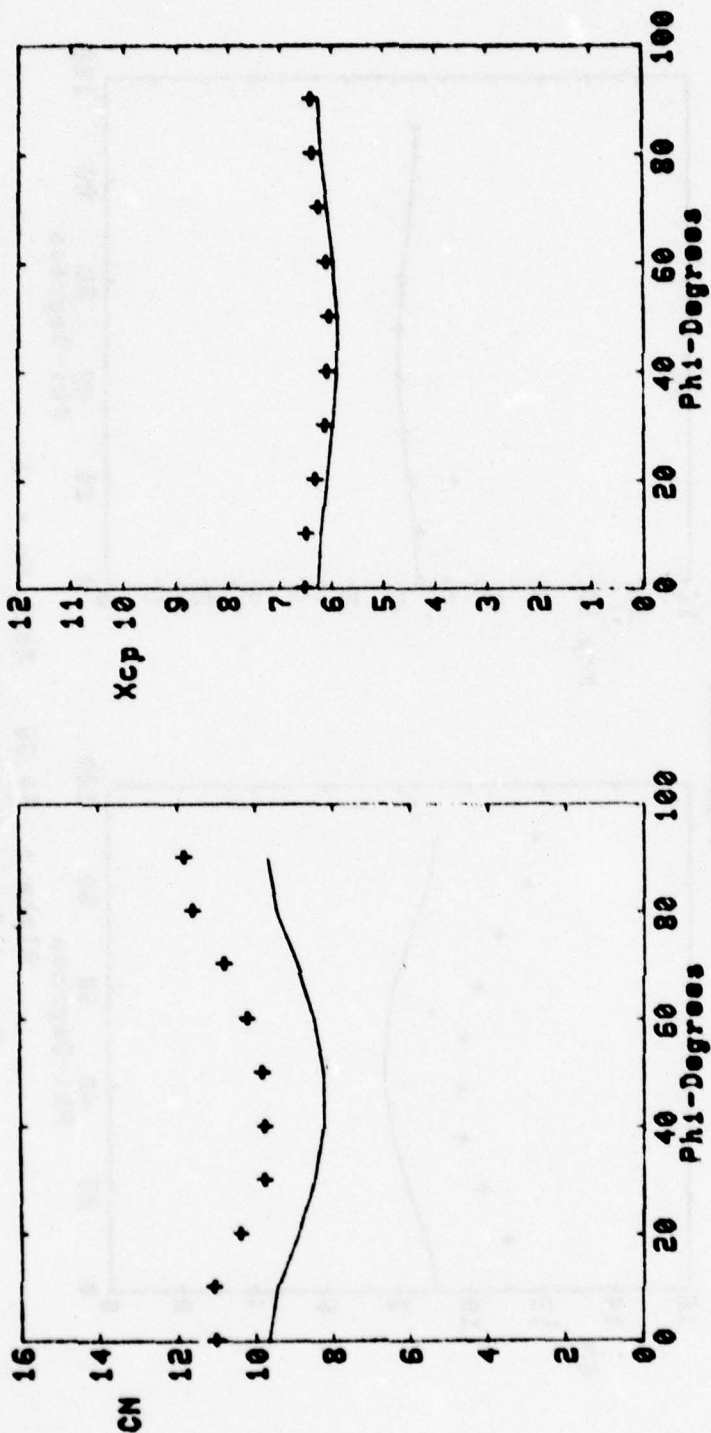
B1T3-1

Mach No. = 1

Alpha = 34.95

Methodology--(-)

Experiment---(+)



Alpha = 34.95 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T3-1

Figure 7b. Modified methodology.

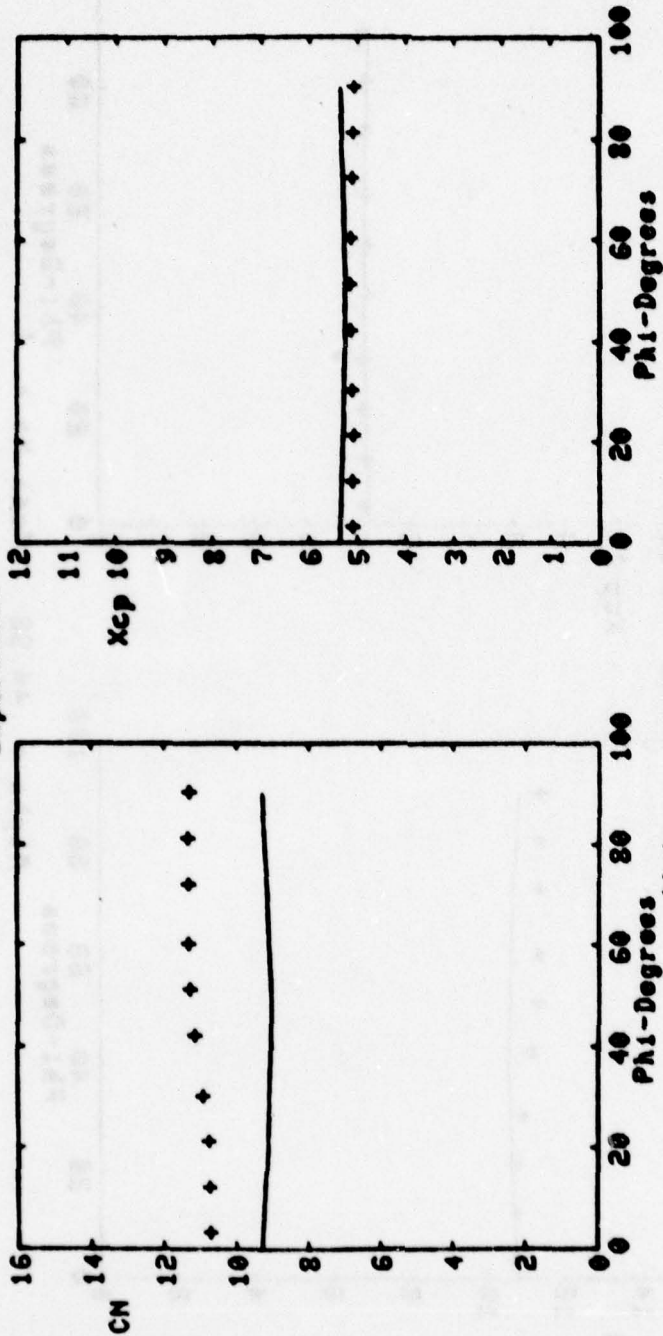
B1T2-3

Mach No. = 1

Alpha = 44.92

Methodology--(-)

Experiment---(+)



Alpha = 44.92 Mach No. = 1
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T2-3

Figure 8a. Original methodology.

B1T2-3
 Mach No. = 1
 Alpha = 44.92
 Methodology--(-)
 Experiment---(+)
 Xcp 10

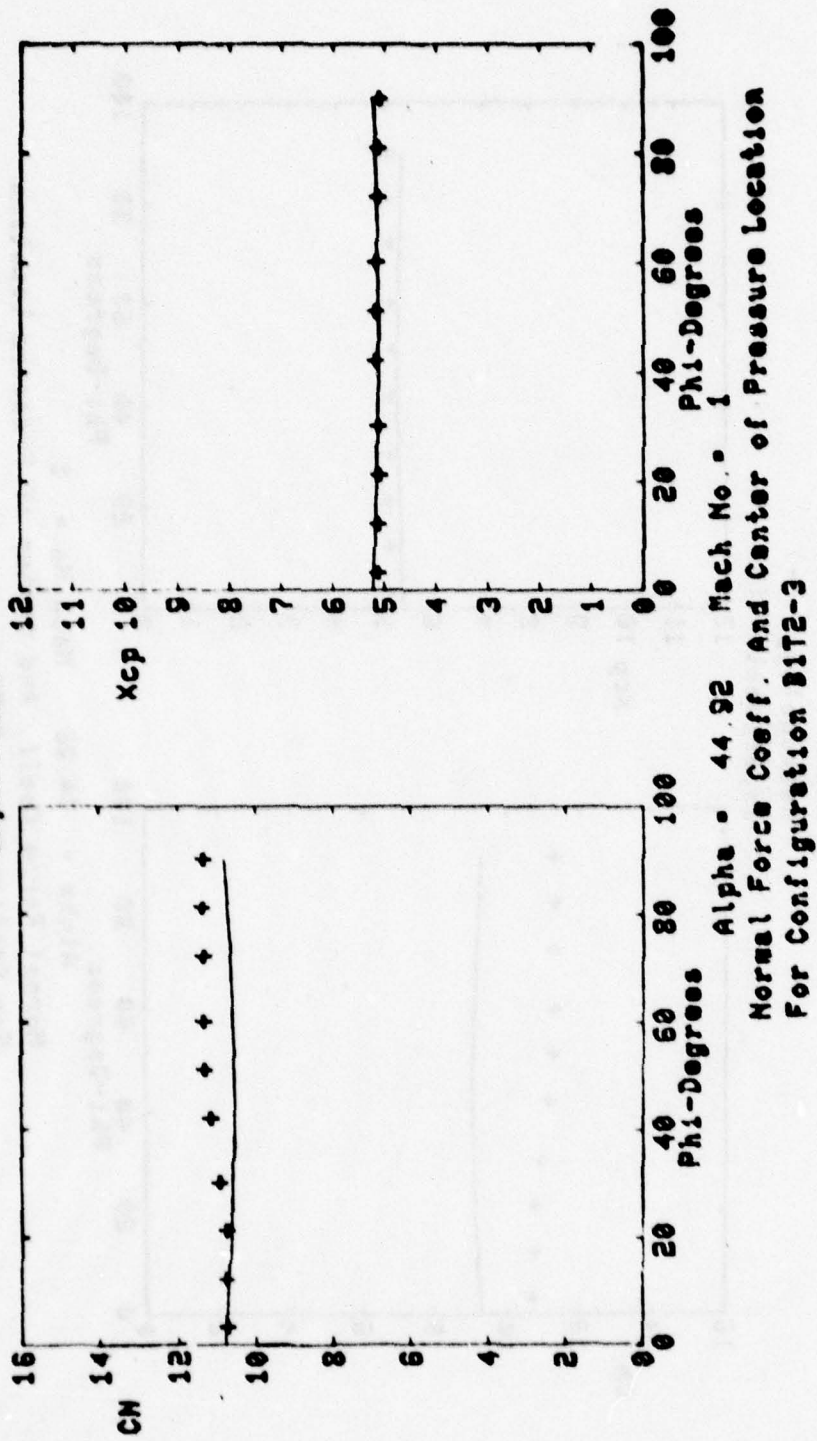
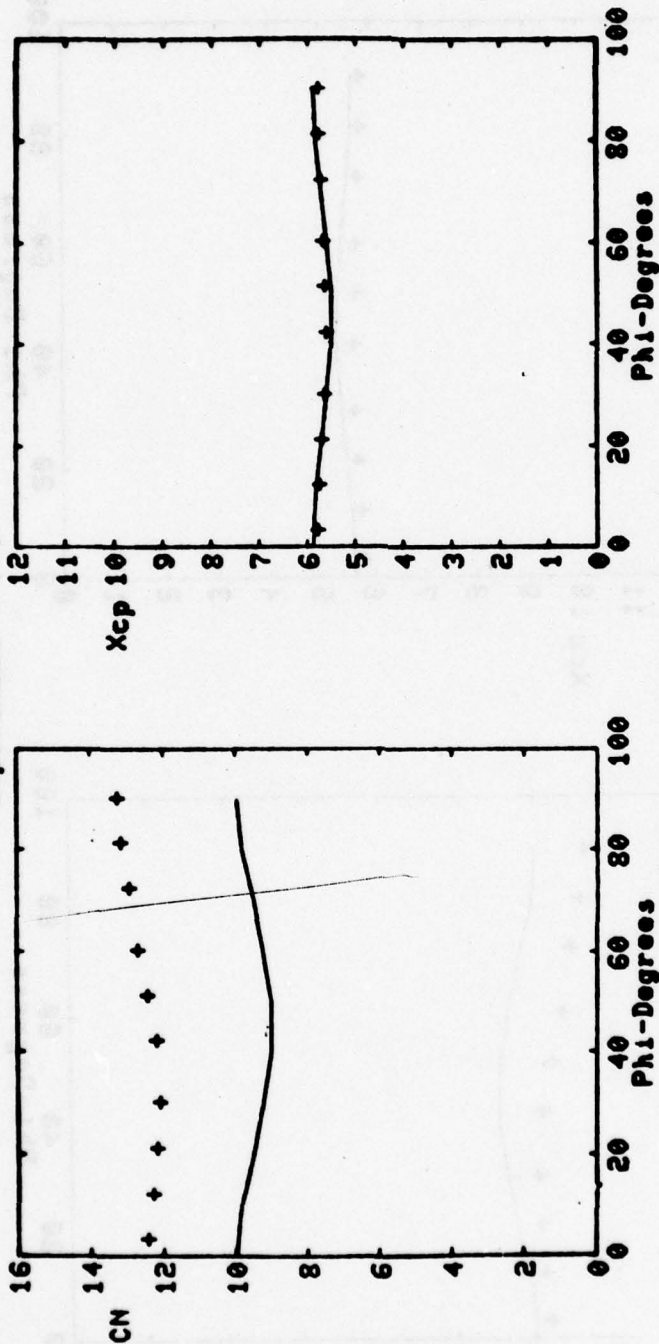


Figure 8b. Modified methodology.

B1T1-4
 Mach No. = 1.2
 Alpha = 44.9
 Methodology---(--)
 Experiment---(+)



Alpha = 44.9 Mach No. = 1.2
 Normal Force Coeff. And Center of Pressure Location
 For Configuration B1T1-4

Figure 9a. Original methodology.

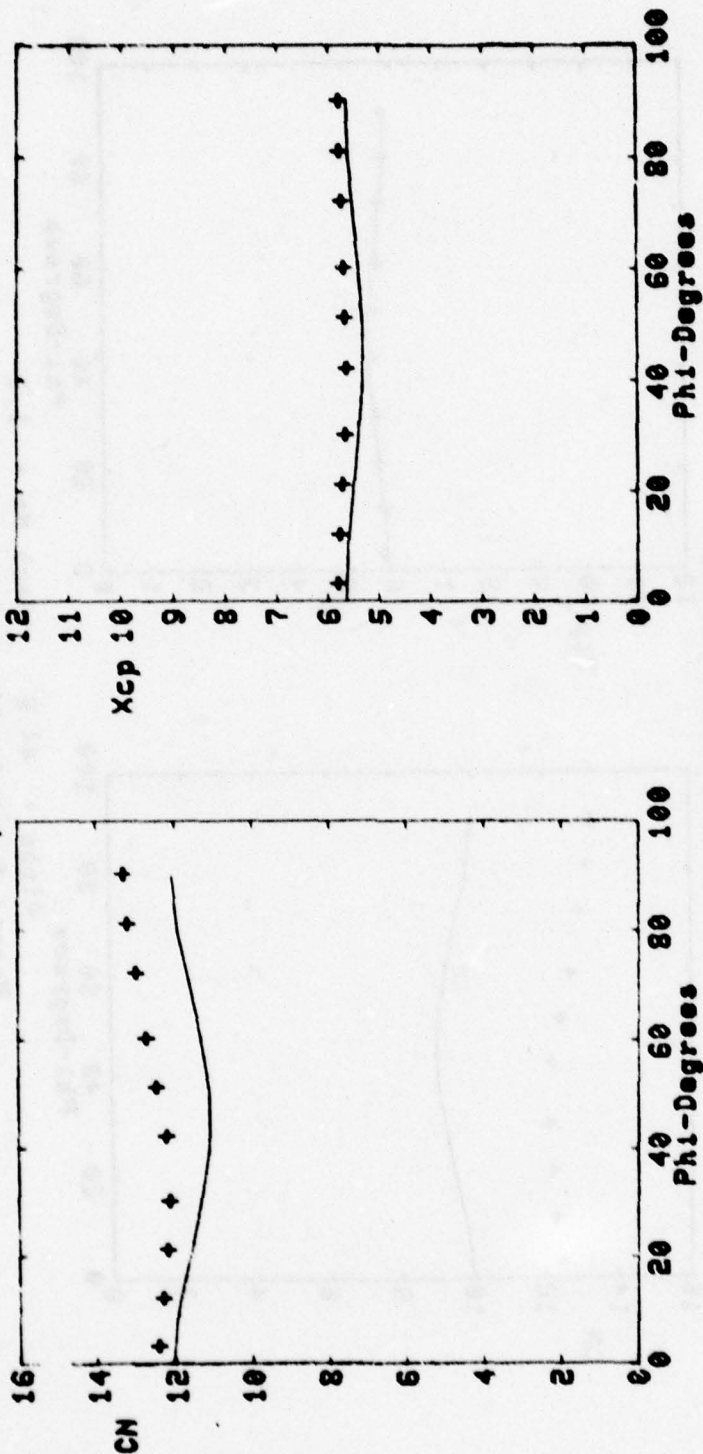
B1T1-4

L. 2

Alpha = 44.9

Methodology--(-)

Experiment---(+)



Alpha = 44.9 Mach No. = 1.2
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T1-4

Figure 9b. Original methodology.

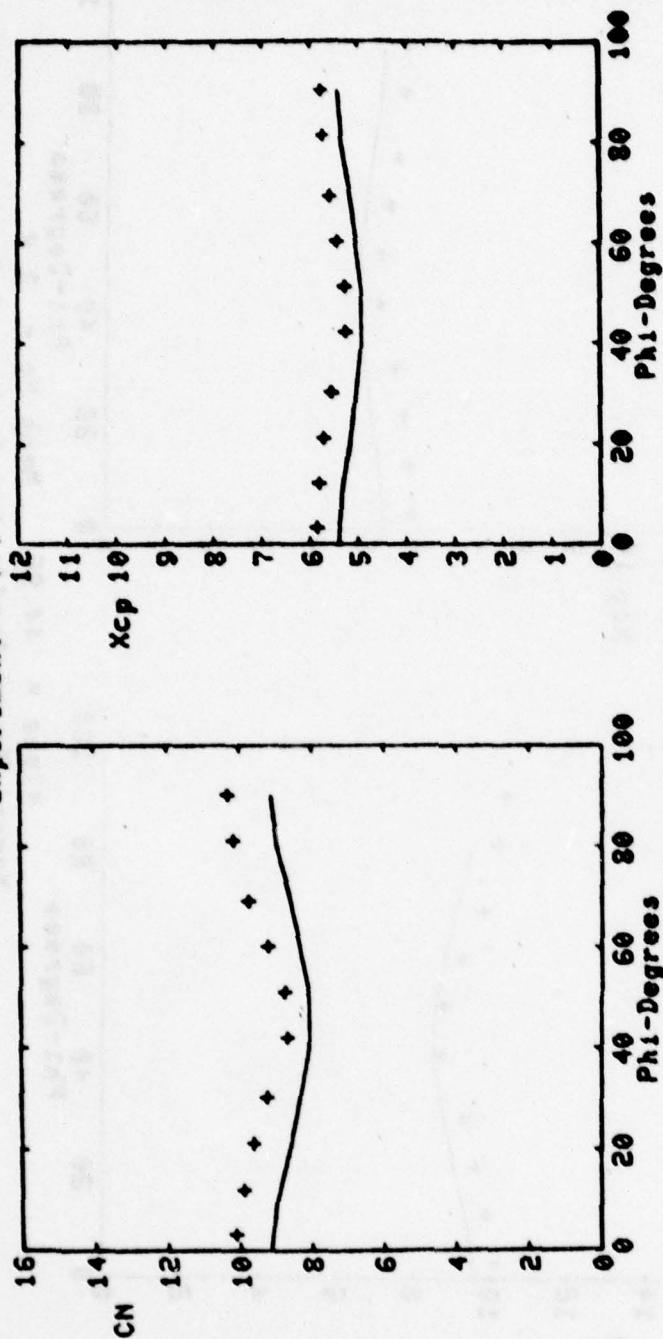
B1T1-4

Mach No. = 0.8

Alpha = 44.95

Methodology--(-)

Experiment---(+)



Alpha = 44.95 Mach No. = 0.8
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T1-4

Figure 10a. Original methodology.

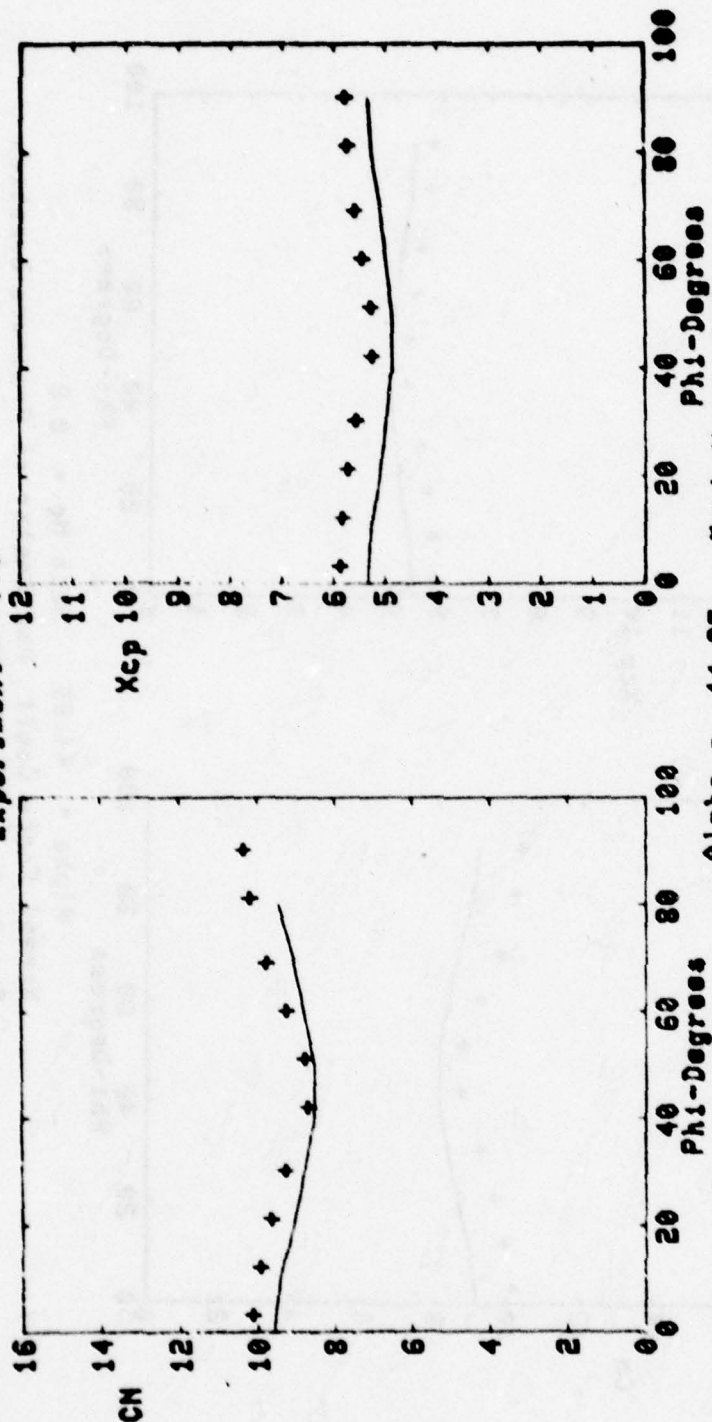
B1T1-4

Mach No. = 0.8

Alpha = 44.95

Methodology--(-)

Experiment---(+)



Alpha = 44.95 Mach No. = 0.8
Normal Force Coeff. And Center of Pressure Location
For Configuration B1T1-4

Figure 10b. Modified methodology.

Appendix A. PROGRAM UTILIZATION

The proper format and sequence for the input cards are shown in Table A-1.

TABLE A-1.

CARD	SYMBOL REFERENCE	FORMAT(FORTRAN)
1	Title card for each configuration	12A6
2	AR,S,CR,LAMDA,ALE	5F10.3
3	LND,LAD,D	3F10.3
4	ALF1,ALF2,DELAF,MACH,RN,OPTPHI, OPTMAC	4F10.3,F13.2,2I2

- AR = Tail aspect ratio (two tail panels joined at root chord)
- S = Tail Semispan including body, $(b + D)/2$, inches
- CR = Tail root chord - Inches
- LAMDA = Tail taper ratio
- ALE = Tail leading edge sweep angle - Degrees
- LND = Nose length - Calibers
- LAD = After-body length - Calibers
- D = Body diameter - Inches
- ALF1 = Beginning angle of attack for angle of attack sweep - Deg.
- ALF2 = Ending angle of attack for angle of attack sweep - Deg.
- DELAF = Angle of attack increment for alpha sweep - Degrees
- MACH = Free stream Mach number
- RN = Reynolds number - /Ft.
- OPTPHI = 1 to calculate aerodynamic coefficients as a function of roll angle. Roll angle is automatically varied between 0° and 90° in increments of 10° . No additional data cards are required. See Sample Configuration 2 Input Data.
- = 0 to delete calculation of aerodynamic coefficients as a function of roll angle
- OPTMAC = 1 allows for multiple Mach numbers for the configuration and angle of attack range determined by the four cards Table A-1. Additional Mach numbers are added after the four cards of Table A-1, one Mach number per card using F10.3 Format
- = 0 for single Mach number only

MULTIPLE CASE CAPABILITY:

Additional configurations can be input simply by repeating the card sequence of Table A-1.

If OPTMAC = 1, however, a blank card must follow the last Mach number card before the program will accept additional configurations.

Table A-2 shows a sample input card arrangement. Using this input card arrangement the program will predict aerodynamic coefficients for sample configuration No. 1 for Mach No. equal .8 and for angles of attack from 0.0 to 45. degrees in 5 degree increments. Since OPTPHI is 0 for sample configuration No. 1, the coefficients will be given versus angle of attack only (roll angle equals 0 degrees). Now, OPTMAC equals 1, therefore additional predictions will be made for the same configuration and angle of attack range for Mach numbers: .9, 1.0, 1.1, 1.2, and 1.3. A blank card follows the Mach number cards for sample configuration No. 1, which signals the program to read additional configurations.

The program then reads the cards for sample configuration No. 2, and computes the predictions of the aerodynamic coefficients and centers of pressure for this configuration. Now, since OPTPHI equals 1 in this case, these predictions will be given as a function of roll angle, for the angle of attack range 0 to 40 degrees. Also, since OPTMAC equals 0 for this case, the predictions will be made for Mach No. equal 2.0 only.

The resulting output for these sample input cards are found in Table A-3.

As a guide for time and storage requirements, the following figures for the CDC 6600 are provided:

Compile Time	-	14 seconds
Execution Time	-	2 seconds
Storage	-	Less than 100K.

TABLE A-3.

I	SAMPLE CONFIGURATION	1	OPTPHI=0, OPTMAC=1			
I						
I	INPUT PARAMETERS					
I						
I	MACH =	.80				
I	TAIL ASPECT RATIO =	1.00				
I	TAIL TAPER RATIO =	0.00				
I	TAIL L-E. SNEEP ANGLE =	75-96 DEGREES				
I	TAIL ROOT CHORD=	7-500				
I	NOSL LENGTH =	3-000 CAL.				
I	AFTER BODY LENGTH =	7-000 CAL.				
I	BODY DIAMETER =	3.75				
I	TAIL SEMI-SPAN(INCLUDING BODY) =	3.75				
I	REYNOLDS NUMBER =	7000000.00				
I						
I	OUTPUT DEFINITIONS					
I						
I	CNB =	BODY ALONE NORMAL FORCE COEFFICIENT				
I	XCPB=	BODY ALONE CENTER OF PRESSURE				
I	CNT =	TAIL ALONE NORMAL FORCE COEFFICIENT				
I	XCPT=	TAIL ALONE CENTER OF PRESSURE				
I	CNT(B)=	TAIL(IN PRESENCE OF BODY) NORMAL FORCE COEFFICIENT				
I	XCPT(B)=	TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)				
I	YCPT(B)=	TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)				
I	XCPT(B-T)=	CENTER OF PRESSURE OF BODY PLUS TAIL I				
I		BODY) MEASURED OUTWARD FROM BODY				
I	CNTP(8-T)=	NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION				
I	CA =	AXIAL FORCE COEFFICIENT				
I						
I	ISOLATED COMPONENTS					
I	I ALPHA I	CNB I XCPB I CNT I XCPT I CNT(B) I				
I	3.00	0.000	2-545	0.000	.651	0.000
I	5.00	.245	2-741	.140	.691	.202
I	11.00	.612	3.181	.307	.743	.431
I	15.00	.961	3.649	.494	.832	.660
I	20.00	.888	3.927	.695	.860	.863
I	25.00	1.151	3.927	.906	.616	1.020
I	30.00	1.652	3.927	1-234	.611	1-236
I	31.00	3.695	3.927	1-220	.617	1-219
I	43.00	5.701	3.927	.967	.622	.975
I	45.00	7.039	3.927	1-213	.628	1-239

SAMPLE CONFIGURATION 1 OPTPHI=0, OPTMAC=1

INPUT PARAMETERS	
MACH =	.90
TAIL ASPECT RATIO =	1.00
TAIL TAPER RATIO =	0.00
TAIL L-E. SHEEP ANGLE =	75.96 DEGREES
TAIL ROOT CHORD =	7.500
NOSE LENGTH =	3.000 CAL.
AFTER BODY LENGTH =	7.000 CAL.
BODY DIAMETER =	3.75
TAIL SEMI-SPAN (INCLUDING BODY) =	3.75
REYNOLDS NUMBER =	7000000.00

OUTPUT DEFINITIONS

CMB =	BODY ALONE NORMAL FORCE COEFFICIENT
KCPB =	BODY ALONE CENTER OF PRESSURE
CNT =	TAIL ALONE NORMAL FORCE COEFFICIENT
KCPT =	TAIL ALONE CENTER OF PRESSURE
CNT(B) =	TAIL (IN PRESENCE OF BODY) NORMAL FORCE COEFFICIENT
KCPT(B) =	TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
YCPT(B) =	TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING CENTER OF PRESSURE OF BODY PLUS TAIL BODY) MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
CNT(B+T) =	NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
CA =	AXIAL FORCE COEFFICIENT

ISOLATED COMPONENTS		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION		BODY TAIL CONFIGURATION	
ALPHA	CMB	KCPB	CNT	KCPT	CNT(B)	KCPT(B)	YCPT(B)	CNT(B+T)	YCPT(B+T)	CA	
0.00	0.000	2.729	0.000	.651	0.000	.651	.335	0.000	.335	.305	
5.00	.246	2.880	.143	.651	.207	.648	.335	.708	.6987	.298	
10.00	.604	3.223	.311	.644	.436	.633	.335	1.534	6.820	.275	
15.00	.894	3.596	.497	.632	.664	.619	.335	2.266	6.956	.238	
20.00	.893	3.835	.696	.621	.864	.613	.316	2.658	7.353	.168	
25.00	1.195	3.835	.903	.616	1.017	.617	.301	3.254	7.197	.166	
30.00	2.782	3.835	1.239	.612	1.241	.624	.282	5.213	6.319	.126	
35.00	4.615	3.835	1.192	.618	1.192	.631	.282	7.050	5.675	.065	
40.00	6.240	3.835	.991	.623	1.004	.638	.282	8.482	5.242	-.018	
45.00	8.114	3.835	1.218	.629	1.253	.644	.282	10.701	5.126	-.120	

EXAMPLE CONFIGURATION 1 OPTPHI=0, OPTMAC=1

INPUT PARAMETERS

MACH = 1.00
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L-E SKEW ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 1.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 7000000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPH = BODY ALONE CENTER OF PRESSURE
 CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPH = TAIL ALONE CENTER OF PRESSURE
 CNT(B) = TAIL IN PRESENCE OF BODY'S NORMAL FORCE COEFFICIENT
 XCPH(B) = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED LEFT FROM ROOT CHORD LEADING EDGE)
 YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCPH(B*) = CENTER OF PRESSURE OF BODY PLUS TAIL BODY MEASURED OUTWARD FROM BODY
 CONFIGURATION (SCALE FROM NOSE)
 CNT(B*) = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA I	ISOLATED COMPONENTS				BODY TAIL CONFIGURATION							
	CNB	XCPH	CNT	XCPH	CNT(B)	XCPH(B)	YCPT(B)	CNT(B*)	XCPH(B*)	YCPT(B*)	CA	I
.00	0.000	2.669	0.000	.652	0.000	.652	.335	0.000	0.000	7.097	.400	I
.00	.246	3.056	.146	.652	.214	.649	.335	.724	.724	7.097	.392	I
.00	.590	3.260	.719	.645	.447	.635	.335	1.544	1.544	6.907	.370	I
.00	.648	3.496	.505	.635	.475	.622	.335	2.046	2.046	7.360	.333	I
.00	.897	3.679	.703	.624	.873	.617	.316	2.677	2.677	7.314	.283	I
.25.00	1.737	3.836	.907	.620	1.821	.621	.301	3.812	3.812	5.716	.285	I
.50.00	3.858	3.834	1.266	.616	1.271	.627	.262	6.336	6.336	5.980	.234	I
.75.00	4.930	4.062	1.147	.621	1.144	.633	.282	7.310	7.310	5.722	.186	I
.90.00	7.082	4.180	1.058	.626	1.045	.640	.262	9.431	9.431	5.429	.130	I
.90.00	8.994	4.317	1.258	.632	1.309	.646	.282	11.654	11.654	5.427	.038	I

AMPLE CONFIGURATION 1 OPTPHI20.0PTWACH1

INPUT PARAMETERS

MACH = 1.10
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L.O. SKEW ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 700000.00

OUTPUT DEFINITIONS

CNP = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPB = BODY ALONE CENTER OF PRESSURE
 XCPB = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPB = TAIL ALONE CENTER OF PRESSURE
 XCPB = TAIL ALONE PRESENCE OF BODY NORMAL FORCE COEFFICIENT
 XCPB = TAIL ALONE PRESENCE OF BODY CHORDWISE CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
 YCPB = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCP(B+T) = CENTER OF PRESSURE OF BODY PLUS TAIL (BODY) MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
 XCP(B+T) = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA I	ISOLATED COMPONENTS				BODY TAIL CONFIGURATION				I	CA
	CNP	XCPB	I	CNT	XCPB	I	CNT(B)	I		
0.00	6.000	2.626	7.000	6.24	0.000	.335	0.000	.335	7.037	.510
5.00	.246	2.788	.146	.634	.211	.431	.722	.7037	.583	
10.00	.569	3.157	.713	.647	.438	.438	1.517	6.941	.480	
15.00	.643	3.558	.404	.610	.540	.535	2.027	7.411	.443	
20.00	.520	3.808	.487	.618	.452	.515	2.679	7.344	.393	
25.00	2.351	3.529	.465	.624	.497	.501	4.399	6.378	.380	
30.00	3.746	4.043	1.318	.621	1.188	.430	6.121	6.045	.358	
35.00	5.427	4.182	1.267	.625	1.261	.282	7.968	5.764	.323	
40.00	7.783	4.281	1.322	.610	1.323	.242	10.408	5.542	.273	
45.00	9.362	4.356	1.350	.610	1.397	.282	12.124	5.500	.211	

AMPLE CONFIGURATION 1 OPTPHI=0 OPTMAC=1

INPUT PARAMETERS

MACH = 1.20
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L.E. SWEEP ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN (INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 700000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPB= BODY ALONE CENTER OF PRESSURE
 CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPT= TAIL ALONE CENTER OF PRESSURE
 CNT(B)= TAIL IN PRESENCE OF BODY NORMAL FORCE
 COEFFICIENT
 XCPT(B) = TAIL (IN PRESENCE OF BODY) CHORDWISE
 CENTER OF PRESSURE/TAIL ROOT CHORD (MEASURED
 AFT FROM ROOT CHORD LEADING EDGE)
 YCPT(B) = TAIL (IN PRESENCE OF BODY) SPANWISE
 CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING
 XCPT(B+T)= CENTER OF PRESSURE OF BODY PLUS TAIL
 BODY) MEASURED OUTWARD FROM BODY
 CONFIGURATION (CAL. FROM NOSE)
 CNT(B+T)= NORMAL FORCE COEFFICIENT OF BODY
 PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

BODY TAIL CONFIGURATION

ALPHA		ISOLATED COMPONENTS				BODY TAIL CONFIGURATION								I				
I	CA	I	CNB	I	XCPB	I	CNT	I	XCPT	I	CNT(B)	I	YCPT(B)	I	CNB(B+T)	I	CA	I
0.00	0.00	0.000	2.431	0.000	.655	0.000	.655	0.000	.335	.335	0.000	.655	.335	0.000	.335	.526		
5.00	.245	2.665	.144	.655	.207	.652	.721	.335	.335	.721	.652	.335	.335	7.008	.335	.318		
10.00	.549	3.191	.307	.649	.431	.641	1.491	.335	.335	1.491	.641	.335	.335	7.013	.335	.095		
15.00	.645	3.741	.486	.640	.649	.630	2.020	.335	.335	2.020	.630	.335	.335	7.474	.335	.459		
20.00	1.159	4.051	.674	.632	.837	.626	2.903	.316	.316	2.903	.626	.316	.316	7.155	.316	.089		
25.00	2.751	4.152	.869	.628	.978	.629	4.780	.301	.301	4.780	.634	.282	.282	6.302	.282	.080		
30.00	4.082	4.253	1.145	.625	1.147	.634	6.407	.282	.282	6.407	.639	.282	.282	6.056	.282	.387		
35.00	5.911	4.355	1.255	.629	1.252	.639	8.432	.282	.282	8.432	.644	.282	.282	5.818	.282	.364		
40.00	8.002	4.456	1.340	.633	1.345	.644	10.682	.282	.282	10.682	.649	.282	.282	5.652	.282	.332		
45.00	9.299	4.557	1.404	.638	1.420	.649	12.100	.282	.282	12.100	.653	.282	.282	5.638	.282	.289		

SAMPLE CONFIGURATION 1 OPTPMI=0.0 OPTMAC=1

INPUT PARAMETERS

MACH = 1.30
 TAIL ASPECT RATIO = 1.00
 TAIL TAPER RATIO = 0.00
 TAIL L.E. SWEEP ANGLE = 75.96 DEGREES
 TAIL ROOT CHORD = 7.500
 NOSE LENGTH = 3.000 CAL.
 AFTER BODY LENGTH = 7.000 CAL.
 BODY DIAMETER = 3.75
 TAIL SEMI-SPAN(INCLUDING BODY) = 3.75
 REYNOLDS NUMBER = 700000.00

OUTPUT DEFINITIONS

CNB = BODY ALONE NORMAL FORCE COEFFICIENT
 XCPB = BODY ALONE CENTER OF PRESSURE
 CNT = TAIL ALONE NORMAL FORCE COEFFICIENT
 XCPT = TAIL ALONE CENTER OF PRESSURE
 CNTB = TAIL(IN PRESENCE OF BODY) NORMAL FORCE COEFFICIENT
 XCPTB = TAIL (IN PRESENCE OF BODY) CHORDWISE CENTER OF PRESSURE/TAIL BODY CHORD (MEASURED AFT FROM ROOT CHORD LEADING EDGE)
 YCPTB = TAIL (IN PRESENCE OF BODY) SPANWISE CENTER OF PRESSURE/TAIL SEMI-SPAN (EXCLUDING BODY)
 XCPB+Y = CENTER OF PRESSURE OF BODY PLUS TAIL BODY MEASURED OUTWARD FROM BODY CONFIGURATION (CAL. FROM NOSE)
 CNTB+Y = NORMAL FORCE COEFFICIENT OF BODY PLUS TAIL CONFIGURATION
 CA = AXIAL FORCE COEFFICIENT

ALPHA	ISOLATED COMPONENTS				BODY TAIL CONFIGURATION							
	CNB	XCPB	CNT	Y	XCPB	YCPTB	CNTB	YCPTB	XCPB+Y	CNTB+Y	CA	Y
0.00	0.000	2.242	0.000	.656	0.000	.656	.328	0.000	.656	.328	.530	.530
5.00	.245	2.540	.142	.656	.200	.653	.328	.713	5.963	.713	.522	.522
10.00	.529	3.204	.304	.650	.411	.642	.328	1.450	7.052	.328	.499	.499
15.00	.647	3.889	.422	.642	.619	.632	.328	1.989	7.503	.328	.463	.463
20.00	1.491	4.252	.670	.633	.805	.628	.315	3.199	6.913	.315	.413	.413
25.00	2.825	4.339	.865	.630	.954	.631	.302	4.828	6.369	.302	.409	.409
30.00	4.417	4.426	1.115	.627	1.115	.636	.287	6.707	6.067	.287	.405	.405
35.00	6.106	4.512	1.241	.631	1.237	.641	.287	8.613	5.895	.287	.395	.395
40.00	7.536	4.599	1.339	.635	1.341	.646	.287	10.213	5.814	.287	.379	.379
45.00	10.261	4.666	1.414	.639	1.424	.650	.287	13.067	5.661	.287	.356	.356

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INPUT PARAMETERS
I
MACH = 2.00
I
TAIL ASPECT RATIO = 1.00
I
TAIL TAPER RATIO = .50
I
TAIL LAC SWEEP ANGLE = 87.17 DEGREES
I
TAIL ROOT CHORD = 5.000
I
NOSE LENGTH = 5.000 CAL.
I
AFTER BODY LENGTH = 6.250 CAL.
I
BODY DIAMETER = 3.75
I
TAIL SEMI-SPACING(INCLUDING FOOT) = 3.75
I
REYNOLDS NUMBER = 6500000.00
I

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CNS = BODY ALONE	NORMAL FORCE COEFFICIENT	1
NCPB = BODY ALONE	CENTER OF PRESSURE	1
CNT = BODY ALONE	NORMAL FORCE COEFFICIENT	1
KCPB = TAIL ALONE	CENTER OF PRESSURE	1
NC1B = TAIL (IN PRESENCE OF BODY)	NORMAL FORCE COEFFICIENT	1
KCP1B = TAIL (IN PRESENCE OF BODY)	CHORDWISE CENTER OF PRESSURE	1
NCPTB = TAIL (IN PRESENCE OF BODY)	CHORDWISE CENTER OF PRESSURE	1
KCP2B = TAIL (IN PRESENCE OF BODY)	CHORD LEADING EDGE AFT FROM ROOT	1
VCPTB = TAIL (IN PRESENCE OF BODY)	SPANWISE CENTER OF PRESSURE	1
NCPTB+T = CENTER OF PRESSURE	TAIL SEMI-SPAN (EXCLUDING BODY)	1
KCPB+T = MEASURED OUTWARD FROM BODY	CONFIGURATION (CAL FROM NOSE)	1
NC1B+T = NORMAL FORCE COEFFICIENT	OF BODY PLUS TAIL CONFIGURATION	1
CA = AXIAL FORCE COEFFICIENT		1

	PHI	I	CM(8)	I	XCPT(2)	I	YCPT(8)	I	MCP(8+T)	I	CM(8+T)	I	CA
	I	FIN 2 I	FIN 4 I	I	FIN 2 I	FIN 4 I	I	FIN 2 I	FIN 4 I	UPPER I	LOWER I	I	I
	I	I	I	I	UPPER I	LOWER I	I	UPPER I	LOWER I	I	I	I	I
0	0.000	0.000	.536	.536	.536	.536	.407	.407	I	I	0.000	.343	
10	0.000	0.000	.536	.536	.536	.536	.408	.407	I	I	0.000	.343	
20	0.000	0.000	.536	.536	.536	.536	.413	.407	I	I	0.000	.343	
30	0.000	0.000	.536	.536	.536	.536	.429	.407	I	I	0.000	.343	
40	0.000	0.000	.536	.536	.536	.536	.458	.407	I	I	0.000	.343	
50	0.000	0.000	.536	.536	.536	.536	.507	.407	I	I	0.000	.343	
60	0.000	0.000	.536	.536	.536	.536	.579	.407	I	I	0.000	.343	
70	0.000	0.000	.536	.536	.536	.536	.681	.407	I	I	0.000	.343	
80	0.000	0.000	.536	.536	.536	.536	.816	.407	I	I	0.000	.343	
90	0.000	0.000	.536	.536	.536	.536	.989	.407	I	I	0.000	.343	

[illegible][illegible]

LPAGE=30,000													
I	CAT(I)		XPT(I)		FIN		YPT(I)		MCP(I+T)		CN(I+T)		I
	FIN 2	FIN 4	FIN 2	FIN 4	FIN 2	FIN 4	FIN 2	FIN 4	UPPER	LOWER	UPPER	LOWER	
0	.967	.567	.587	.587	.587	.587	.587	.587	6.065	6.065	8.058	8.058	342
1	.962	1.109	.584	.584	.587	.587	.587	.587	6.064	6.064	8.057	8.057	343
2	.921	1.149	.584	.584	.587	.587	.587	.587	6.025	6.025	8.050	8.050	344
3	.910	1.126	.584	.584	.586	.586	.586	.586	5.991	5.991	7.970	7.970	345
4	.840	1.021	.583	.583	.585	.585	.585	.585	5.992	5.992	7.970	7.970	346
5	.845	1.064	.576	.576	.587	.587	.587	.587	5.992	5.988	7.970	7.970	347
6	.837	.787	.587	.587	.576	.576	1.000	1.000	5.990	5.991	7.970	7.970	348
7	.102	.524	.586	.586	.585	.585	1.000	1.000	6.025	6.026	8.050	8.050	349
8	.896	.426	.586	.586	.584	.584	1.000	1.000	6.025	6.064	8.057	8.057	350
9	.900	0.400	.586	.586	.584	.584	1.000	1.000	6.025	5.965	8.058	8.058	351

PHI	FIN 2	FIN 4	FIN 6	FIN 8	FIN 10	FIN 12	FIN 14	FIN 16	FIN 18	FIN 20	FIN 22	FIN 24	FIN 26	FIN 28	FIN 30	FIN 32	FIN 34	FIN 36	FIN 38	FIN 40	FIN 42	FIN 44	FIN 46	FIN 48	FIN 50	FIN 52	FIN 54	FIN 56	FIN 58	FIN 60	FIN 62	FIN 64	FIN 66	FIN 68	FIN 70	FIN 72	FIN 74	FIN 76	FIN 78	FIN 80	FIN 82	FIN 84	FIN 86	FIN 88	FIN 90	FIN 92	FIN 94	FIN 96	FIN 98	FIN 100	FIN 102	FIN 104	FIN 106	FIN 108	FIN 110	FIN 112	FIN 114	FIN 116	FIN 118	FIN 120	FIN 122	FIN 124	FIN 126	FIN 128	FIN 130	FIN 132	FIN 134	FIN 136	FIN 138	FIN 140	FIN 142	FIN 144	FIN 146	FIN 148	FIN 150	FIN 152	FIN 154	FIN 156	FIN 158	FIN 160	FIN 162	FIN 164	FIN 166	FIN 168	FIN 170	FIN 172	FIN 174	FIN 176	FIN 178	FIN 180	FIN 182	FIN 184	FIN 186	FIN 188	FIN 190	FIN 192	FIN 194	FIN 196	FIN 198	FIN 200	FIN 202	FIN 204	FIN 206	FIN 208	FIN 210	FIN 212	FIN 214	FIN 216	FIN 218	FIN 220	FIN 222	FIN 224	FIN 226	FIN 228	FIN 230	FIN 232	FIN 234	FIN 236	FIN 238	FIN 240	FIN 242	FIN 244	FIN 246	FIN 248	FIN 250	FIN 252	FIN 254	FIN 256	FIN 258	FIN 260	FIN 262	FIN 264	FIN 266	FIN 268	FIN 270	FIN 272	FIN 274	FIN 276	FIN 278	FIN 280	FIN 282	FIN 284	FIN 286	FIN 288	FIN 290	FIN 292	FIN 294	FIN 296	FIN 298	FIN 300	FIN 302	FIN 304	FIN 306	FIN 308	FIN 310	FIN 312	FIN 314	FIN 316	FIN 318	FIN 320	FIN 322	FIN 324	FIN 326	FIN 328	FIN 330	FIN 332	FIN 334	FIN 336	FIN 338	FIN 340	FIN 342	FIN 344	FIN 346	FIN 348	FIN 350	FIN 352	FIN 354	FIN 356	FIN 358	FIN 360	FIN 362	FIN 364	FIN 366	FIN 368	FIN 370	FIN 372	FIN 374	FIN 376	FIN 378	FIN 380	FIN 382	FIN 384	FIN 386	FIN 388	FIN 390	FIN 392	FIN 394	FIN 396	FIN 398	FIN 400	FIN 402	FIN 404	FIN 406	FIN 408	FIN 410	FIN 412	FIN 414	FIN 416	FIN 418	FIN 420	FIN 422	FIN 424	FIN 426	FIN 428	FIN 430	FIN 432	FIN 434	FIN 436	FIN 438	FIN 440	FIN 442	FIN 444	FIN 446	FIN 448	FIN 450	FIN 452	FIN 454	FIN 456	FIN 458	FIN 460	FIN 462	FIN 464	FIN 466	FIN 468	FIN 470	FIN 472	FIN 474	FIN 476	FIN 478	FIN 480	FIN 482	FIN 484	FIN 486	FIN 488	FIN 490	FIN 492	FIN 494	FIN 496	FIN 498	FIN 500	FIN 502	FIN 504	FIN 506	FIN 508	FIN 510	FIN 512	FIN 514	FIN 516	FIN 518	FIN 520	FIN 522	FIN 524	FIN 526	FIN 528	FIN 530	FIN 532	FIN 534	FIN 536	FIN 538	FIN 540	FIN 542	FIN 544	FIN 546	FIN 548	FIN 550	FIN 552	FIN 554	FIN 556	FIN 558	FIN 560	FIN 562	FIN 564	FIN 566	FIN 568	FIN 570	FIN 572	FIN 574	FIN 576	FIN 578	FIN 580	FIN 582	FIN 584	FIN 586	FIN 588	FIN 590	FIN 592	FIN 594	FIN 596	FIN 598	FIN 600	FIN 602	FIN 604	FIN 606	FIN 608	FIN 610	FIN 612	FIN 614	FIN 616	FIN 618	FIN 620	FIN 622	FIN 624	FIN 626	FIN 628	FIN 630	FIN 632	FIN 634	FIN 636	FIN 638	FIN 640	FIN 642	FIN 644	FIN 646	FIN 648	FIN 650	FIN 652	FIN 654	FIN 656	FIN 658	FIN 660	FIN 662	FIN 664	FIN 666	FIN 668	FIN 670	FIN 672	FIN 674	FIN 676	FIN 678	FIN 680	FIN 682	FIN 684	FIN 686	FIN 688	FIN 690	FIN 692	FIN 694	FIN 696	FIN 698	FIN 700	FIN 702	FIN 704	FIN 706	FIN 708	FIN 710	FIN 712	FIN 714	FIN 716	FIN 718	FIN 720	FIN 722	FIN 724	FIN 726	FIN 728	FIN 730	FIN 732	FIN 734	FIN 736	FIN 738	FIN 740	FIN 742	FIN 744	FIN 746	FIN 748	FIN 750	FIN
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1      PROGRAM MAIN(TAPES,TAPE6)
2
3      THIS PROGRAM USES AN AERODYNAMIC METHODOLOGY DEVELOPED BY THE
4      MARTIN MARIETTA CORP. TO PREDICT AERODYNAMIC COEFFICIENTS OF
5      MISSILES WITH LOW ASPECT RATIO TAILS AT LOW AND HIGH ANGLES OF
6      ATTACK AND ARBITRARY ROLL ANGLES.
7
8      THE INPUT PARAMETERS AND THEIR LIMITS FOR THIS METHOD ARE:
9
10     MACH = MACH NUMBER .8 TO 3.0
11     ALPHA = ANGLE OF ATTACK (DEG) 0. TO 180 (0 TO 45 FOR ROLL)
12     ALE = TAIL LEADING EDGE SWEEP ANGLE (DEG) 0 TO 70 DEG
13     LAD = AFTER BODY LENGTH IN CAL. 6 TO 18
14     LND = NOSE LENGTH IN CAL. 1.5 TO 3.5
15     LMD = TAIL TAPER RATIO 0 TO 1
16     LMDA = TAIL ASPECT RATIO (TWO PANELS) .5 TO 3.5
17     AP = BEGINNING ALPHA FOR DESIRED ALPHA SWEEP (DEG)
18     ALF1 = END POINT FOR ALPHA SWEEP (DEG)
19     ALF2 = ALPHA INCREMENT FOR ALPHA SWEEP (DEG)
20     DELAF = REYNOLDS NUMBER/FT.
21     RN = TAIL SEMI SPAN INCLUDING BODY, (B*D)/2, INCHES
22     S = TAIL ROOT CHORD INCHES
23     CR = BODY DIAMETER INCHES
24     OPTPHI = 0 GIVES NO PREDICTIONS VS. ROLL ANGLE
25
26     = 1 GIVES AERODYNAMIC COEFFICIENTS AND CENTER OF
27     PRESSURE AS A FUNCTION OF ROLL ANGLE
28     OPTMAC = 1 ALLOWS FOR MULTIPLE MACH NO. CALCULATIONS FOR
29     A GIVEN CONFIGURATION
30
31     = 0 CALCULATIONS FOR SINGLE MACH NO. ONLY
32
33     INTEGER OPTPHI,OPTMAC
34     DIMENSION ANAME(12)
35     REAL MACH,LAMDA,LND,LAD,18T
36     GO TO 11
37
38     1 IF(OPTMAC.EQ. 1) GO TO 2
39     11 READ(5,208) (ANAME(I),I=1,12)
40     IF(OPT5) 400,25
41     25 READ(5,200) AR,S,CR,LAMDA,ALE
42     READ(5,201) LND,LAD,0
43     15 READ(5,202) ALF1,ALF2,DELAF,MACH,RN,OPTPHI,OPTMAC
44     GO TO 3
45
46     2 READ(5,203) MACH
47     IF(OPT5) 400,26
48     26 IF(MACH.EQ. 0.) GO TO 11
49     3 WRITE(6,140) (ANAME(I),I=1,12)
50     WRITE(6,117)
51     WRITE(6,109)
52     WRITE(6,110)
53     WRITE(6,111) MACH
54     WRITE(6,112) AR
55     WRITE(6,113) LAMDA
56     WRITE(6,114) ALE
57     WRITE(6,115) CR
58     WRITE(6,116) LND

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```

60  *PI*(6.117) LAD
    *PI*(6.150) D
    *PI*(6.151) S
    *PI*(6.112) PN
    *PI*(6.110)
    *PI*(6.115)
    *PI*(6.141)
    *PI*(6.141)
    *PI*(6.119)
    *PI*(6.120)
    *PI*(6.110)
    *PI*(6.121)
    *PI*(6.122)
    *PI*(6.120)
    *PI*(6.120)
    *PI*(6.126)
    *PI*(6.126)
    *PI*(6.127)
    *PI*(6.128)
    *PI*(6.161)
    *PI*(6.129)
    *PI*(6.130)
    *PI*(6.131)
    *PI*(6.162)
    *PI*(6.132)
    *PI*(6.133)
    *PI*(6.134)
    *PI*(6.135)
    *PI*(6.130)
    *PI*(6.119)
    *PI*(6.119)
    5  PI = 3.1415926535
    CIO = 21/100
    CT = 45*CR*(1+LAWCA)*(S-0/2.)
    CRASP = 3.14159*(0/2)*0.2
    *RATIO = ST/SEASE
    *LND**2 +25
    *ATE = ((2.*PI*(PI*(10-.5)*ASIN(-LND/PI)*LND))*.D**2*LAD*.D*.2.*
    1PI*(0/2.)
    ANCP=ANCIS/CRASP
    COUNT = 0
    KIT = 2
    ALPH = ALF1
    IF(COPTPHI .GT. 1) GO TO 5
    *PI*(6.142)
    *PI*(6.106)
    *PI*(6.107)
    *PI*(6.142)
    5  CALL AXIAL((LAD*LND*MACH*ANCP*ALPHA*PN,CA)
    CALL XCPSTI((ALPHA*LAWDA*MACH*AP*.D*S*NCPEI)
    XCP1 = (LND*LAD*CR/D)* XCPST*CR/D
    CALL CNBOD((LAD*LND*MACH*ALPHAD*CNB*PN)
    CALL XCP*CD(LAD*LND*.D*MACH*ALPHAD*CNB*PN)
    IF(COPTPHI .GT. 1) GO TO 10
    CALL CN1((ALPHA*LAWDA*MACH*AP*CNT)
    CALL XCP1I((ALPHA*LAWDA*MACH*AP*MCPT)
    IF(ALPHA .GT. 45.) GO TO 300
    PHI = 90.

```

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000670
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001040
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001120
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001170
001180
001190
001200
001210
001220
001230

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115 CALL CNTPHI(MACH,AR,LAMDA,D,S,ALPHA,PHI,CR,ALE,CNTB,
    CALL I8TTLAMDA,MACH,AR,ALPHA,PHI,S,D,IBT)
    CALL XCP1B1(MACH,AR,LAMDA,D,S,CR,ALPHA,PHI,XCPTB1,XCPTB2)
    CALL YCPT3(LAMDA,PHI,ALPHA,MACH,S,D,CR,YCPT3)
    CMPT = CNB + 2 * CNTB-ARATIO + IBT
    XCPT1 = LAD-LND-CR/D + XCPTB1-CR/D
    GO TO 16
120 300 WRITE(6,204) ALPHA,CNB,XCPB,CNT,XCPT,CA
    GO TO 36
125 16 XCPBT = (CNB-XCPB + 2 * CNTB-ARATIO-XCPT1
    WRITE(6,108) ALPHA,CNB,XCPB,CNT,XCPT,XCPTB1,YCPT,CMBT,XCPBT,
    1CA
    30 ALPHA = ALPHA + DELAF
    IF(ALPHA .GT. ALF2) GO TO 1
    KOUNT = KOUNT + 1
    IF(KOUNT .EQ. 50 .AND. OPTPHI .EQ. 0) GO TO 4
    GO TO 5
130 10 IF(KIT .EQ. 0) WRITE(6,140)
    WRITE(6,141)
    WRITE(6,101) ALPHA
    WRITE(6,105)
    WRITE(6,102)
    WRITE(6,102)
    WRITE(6,104)
    WRITE(6,105)
    KIT = KIT + 1
    IF(KIT .EQ. 3) KIT = 0
    PHI = 0.
    DO 20 I=1,10
    PHI1 = 180. - PHI
    PHI2 = PHI + 90.
    PHI3 = PHI
    PHI4 = 90. - PHI
    CALL CNTPHI(MACH,AR,LAMDA,D,S,ALPHA,PHI1,CR,ALE,CNTB1)
    CALL CNTPHI(MACH,AR,LAMDA,D,S,ALPHA,PHI2,CR,ALE,CNTB2)
    CALL CNTPHI(MACH,AR,LAMDA,D,S,ALPHA,PHI3,CR,ALE,CNTB3)
    CALL CNTPHI(MACH,AR,LAMDA,D,S,ALPHA,PHI4,CR,ALE,CNTB4)
    CALL XCP1B1(MACH,AR,LAMDA,D,S,CR,ALPHA,PHI1,XCPT1,XCPT11)
    CALL XCP1B1(MACH,AR,LAMDA,D,S,CR,ALPHA,PHI2,XCPT12,XCPT12)
    CALL XCP1B1(MACH,AR,LAMDA,D,S,CR,ALPHA,PHI3,XCPT13,XCPT13)
    CALL XCP1B1(MACH,AR,LAMDA,D,S,CR,ALPHA,PHI4,XCPT14,XCPT14)
    CALL YCPT3(LAMDA,PHI1,ALPHA,MACH,S,D,CR,YCPT11)
    CALL YCPT3(LAMDA,PHI2,ALPHA,MACH,S,D,CR,YCPT12)
    CALL YCPT3(LAMDA,PHI3,ALPHA,MACH,S,D,CR,YCPT13)
    CALL YCPT3(LAMDA,PHI4,ALPHA,MACH,S,D,CR,YCPT14)
    IF(ALPHA .GT. 90.) GO TO 35
    XCT1=LAD-LND-CR/D + XCPT11-CR/D
    XCT2=LAD-LND-CR/D + XCPT12-CR/D
    XCT3=LAD-LND-CR/D + XCPT13-CR/D
    XCT4=LAD-LND-CR/D + XCPT14-CR/D
    XCTU1=LAD-LND-CR/D + XCPTJ1-CR/D
    XCTU2=LAD-LND-CR/D + XCPTJ2-CR/D
    XCTU3=LAD-LND-CR/D + XCPTJ3-CR/D
    XCTU4=LAD-LND-CR/D + XCPTJ4-CR/D
    GO TO 36
135 35 XCT1=LAD-LND-XCPT11-CR/D
140
145
150
155
160
165
170
201800

```


[illegible]

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230 PHIPRM = 90.-PHI
   PPRM = 50.-PHIP
   A3=(16000.-PHIPRM-16000.-PHIPRM**2+400.-PHIPRM**3)/(400.-PHIPRM**3)
   PPRM=40.-PPRM**2+PPRM**3)
   A4=(40.-PPRM**3)/PHIPRM-1200.-PHIPRM*(PPRM**2)-(PPRM**3)+
   PHIPRM**2+1200.-PPRM*(PHIPRM**2)+(PPRM**2)*(PHIPRM**3)-40.-
   PPRM*(PHIPRM**3)/(400.-PHIPRM-40.-PPRM**2+PPRM**3)
   RTBPM = RTEP*SIN(PHIP-.0174532)
   A = RTEPMP-RTBO
   CALL LOOK3(P,RT,9.,ALPHA,BEALFT,9.,ALE,BEALFT,9.,MACH,BEMACT,3,
   .IX,IY,I2,I1)
   RTE = RTBO + A*A3 + B *A4
   GO TO 80
140 RTE = RTEP*SIN(PHIP-.0174532)
   GO TO 80
90 JFLAG = 0
   RTB1 = RTB
   MACH = 1.75
   MFLAG = 1
   GO TO 40
50 JFLAG = 1
   MACTP = MACH
   MACH = 1.2
   GO TO 30
100 KFLAG = 0
   MACH = MACTP
   RTB2 = RTB
   GO TO 110
40 CALL LOOK2(RTEP,RTB2,3,AR,RTEPAR,3,LAMDA,RTBPLD,3,IX,IY,I1)
   IF(PHI .LT. 4.) GO TO 120
   RTB45 = RTEP*SIN(45.-.0174532)
   A = RTB45-RTBO
   CALL LOOK3(B,RT,5.,ALPHA,BEALFT,5.,ALE,BEALFT,5.,MACH,BEMACT,4,I
   .IX,IY,I2,I1)
   PHIP = 45.
   PHIPRM = 50.-PHI
   PPRM = 90.-PHIP
   A3=(16000.-PHIPRM-16000.-PHIPRM**2+400.-PHIPRM**3)/(400.-PHIPRM**3)
   PPRM=40.-PPRM**2+PPRM**3)
   A4=(40.-PPRM**3)/PHIPRM-1200.-PHIPRM*(PPRM**2)-(PPRM**3)+
   PHIPRM**2+1200.-PPRM*(PHIPRM**2)+(PPRM**2)*(PHIPRM**3)-40.-
   PPRM*(PHIPRM**3)/(400.-PHIPRM-40.-PPRM**2+PPRM**3)
   RTB = RTBO + A*A3 + B *A4
   GO TO 80
120 RTE = RTEP*SIN(PHIP-.0174532)
   GO TO 80
200 IF(ALPHA .GT. 30.) GO TO 210
   ALF = ALPHA + 10.
   A2=2.07752E-07*ALF**4 + 1.72193E-05*ALF**3 + 6.24467E-04*ALF**2
   + .016458069*ALF + .087604485
   A1 = 4.66769E-07*ALF**4 - 4.22299E-05*ALF**3 + 2.32986E-04*ALF**2
   + .6936E-03*ALF + .98159845
   CALL LOOK1(KTY,KTF,US,KTBD,11,IX,I1)
   RTBO = AC + A1*KTE
   IF(IFLAG .EQ. 1) GO TO 290
   IF(IFLAG .EQ. 1) GO TO 300

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```

280 GO TO 25
290 210 ALF = ALPHA + 10.
    A0 = 4.5799E-12*ALF**6 - 2.30809E-09*ALF**5 + 3.96812E-07*ALF**4
    A1 = 2.15272E-05*ALF**3 - 8.10606E-04*ALF**2 + .092902183*ALF
    A2 = -.85855362
    A3 = 1.67133E-11*ALF**6 - 9.5912E-09*ALF**5 + 2.09288E-06*ALF**4
    A4 = 2.19478E-04*ALF**3 + .011664495*ALF**2 - .303221946*ALF
    A5 = 3.0674E-046
295 CALL LOOK1(K15,RTPT,DS,K1PDS,11,1X,1)
    A2 = -2.16611E-11*ALF**6 + 1.21153E-08*ALF**5 - 2.53877E-06*ALF**4
    A3 = -2.4641E-04*ALF**3 + .01114855*ALF**2 + .217380211*ALF
    A4 = -1.28277255
    CALL LOOK2(RTP2,RTPT,12,MACH,RTPT2*12,LAMDA,RTPT2*3,1X,1Y,1)
    RTPT2 = RTPT2-LAMDA
    RTPT = A0 + A1*RTPT + A2*RTPT2
    IF(LFLAG.EQ.1) GO TO 300
    IF(LFLAG.EQ.1) GO TO 290
    GO TO 280
300 220 ALF = ALPHA + 10.
    A0 = 4.5799E-12*ALF**6 - 2.30809E-09*ALF**5 + 3.96812E-07*ALF**4
    A1 = 2.15272E-05*ALF**3 - 8.10606E-04*ALF**2 + .092902183*ALF
    A2 = -.85855362
    A3 = 1.67133E-11*ALF**6 - 9.5912E-09*ALF**5 + 2.09288E-06*ALF**4
    A4 = 2.19478E-04*ALF**3 + .011664495*ALF**2 - .303221946*ALF
    A5 = 3.0674E-046
310 GO TO 220
230 IF LFLAG = 1
    MACH2 = MACH
    MACH = 1.2
    GO TO 290
315 290 IF LAG = 0
    RTPT = RTPT
    MACH = 1.75
    LFLAG = 1
    GO TO 220
320 300 LFLAG = 0
    MACH = MACH2
    RTPT2 = RTPT
    RTPT = RTPT*((MACH-1.2)/.55)*(RTPT2-RTPT)
    GO TO 25
325 600 DCP = D/CR
    CALL PHCC(ALPHA,MACH,DCR,PHC1)
    PHC = PHC1*240
    PHI = (PHI-90.)*240
    A = (1.-(1.-(PHC**2))**2)/(PHC**2)/(PI/2.)*2/(PI/2.)*PHI**2
    A = (PHI*(1.-(PHC**2))-(PHC*(PI/2.)))/(PI/2.)*PHI**2+((1.-(PHC
    A = -1.-(PI/2.))/(PI/2.)*PHI**3)
    PHI = PHI/240.
    IF(MACH.LT.1.2) GO TO 410
    CALL LOOK3(RPM,APPM,RT,19,10,MACH,RPM,19,ALPHA,APPM,10,LAMDA,
    APPM,19,1X,1Y,1Z,1)
    IF(APPM.LT.1) GO TO 420
    CALL LOOK4(RT,RTPT,19,10,MACH,RTPT,19,ALPHA,RTPTA,10,AR,
    RTPTA,19,1X,1Y,1Z,1)
    APPM = APPM*RTPT
    GO TO 620

```


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04/27/78 09.19.41.

FIN 4.2*74355

SUBROUTINE CATP=1 74/74 OPT=1

006180
006190
006200
006210

610 RPR = 0.
620 RTR = RYTCOA + RPR**B
GO TO 110
END

345

46

PAGE 4

04/27/78 09.23.25.

FTN 4.2-7A355

007930
007940

OPT=1

74/74

SUBROUTINE CNTY

GO TO 98
END


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115      2.510..505..517..323..326..460..467..501..593..537..330..320..310. 009090
      3.422..406..509..550..485..337..315..360..423..500..560..580..605. 009100
      4000..330..445..475..485..485..485..485..485..485..485..485..485. 009110
      5.465..470..470..470..470..470..470..470..470..470..470..470..470. 009120
      6.390..433..457..470..477..477..477..477..477..477..477..477..477. 009130
      7.495..500..510..423..423..423..423..423..423..423..423..423..423. 009140
      8.485..493..493..493..493..493..493..493..493..493..493..493..493. 009150
      X=ASIN(SQRT(1.-Y**2))
      Y=ASIN(SQRT(1.-X**2))
      Z=18
      IF(X.GT.7.) WRITE (6,900) X
      IF(Z.GT.1.) WRITE (6,902) Z
      IF(X.GT.1.0) GO TO 1
      CALL LOOK3(CLEAR,PAR1,15,7,X,YT1,15,Y,YT1,7,Z,YT1,4,IX,IV,IZ,1)
      IF(Y.GT.4.) WRITE (6,901) Y
      CALL LOOK3(CLEAR,PAR2,5,5,X,YT2,5,Z,YT2,5,Z,YT2,4,IX,IV,IZ,1)
      CLEAR=CLAR*AR
      RETURN
1      CALL LOOK3(CLEAR,PAR3,15,7,X,AT1,15,Y,YT1,7,Z,YT1,4,IX,IV,IZ,1)
      IF(Y.GT.4.) WRITE (6,901) Y
      CALL LOOK3(CLEAR,PAR4,5,5,X,YT2,5,Z,YT2,5,Z,YT2,4,IX,IV,IZ,1)
      CLEAR=CLAR*AR
      RETURN
900  FORMAT (1X,'EXTRAPOLATION REQUIRED',*10HAR*ETA = F10.4)
901  FORMAT (1X,'EXTRAPOLATION REQUIRED',*11HAR*TANSM = F10.4)
902  FORMAT (1X,'EXTRAPOLATION REQUIRED',*12HAR*TAPEX RATIO = F10.4)
      END

```


[illegible]

SUBROUTINE CNBOD 76/76 OPT=1

```

018500      * (16.00000/PI.000)*CNP12
018510      RETURN
018520      20 IF(MACH.LT.1.0) GO TO 90
018530      110 CALL LOOK3(CNA,CNAT,13.0,MACH,CNAM,13.0,AD,CNALD,4.0,
018540      $,INVL,12.0)
018550      GO TO 120
018560      30 CNAT=CNA
018570      IFLAG=0
018580      MACH=1.5
018590      JFLAG=1
018600      GO TO 110
018610      40 CNAT=CNA
018620      MACH = MACHT
018630      JFLAG=0
018640      CNAT=CNAT-(CNAT-CNAT)*0.5*(MACH)/.3
018650      GO TO 50
018660      50 IFLAG = 1
018670      MACHT=MACH
018680      MACH = 1.2
018690      GO TO 10
018700      75 A=ALPHA*PAC
018710      CNE=SI*(2.000)*C0*(A/2.0)*CEC*U*(SP/SPFF)*(SIN(A))**.2
018720      RETURN
018730      END

```



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011870

140 CALL LOG10(CELX,CFLXT,WACHC,DFLA#23,I#*J)
      DELV = CELAOLD
      X20 = XC+DFLX
      A = ALPHA
      A0 = 1-*(07+A**2/26000*-21-A**2/2400.)
      A1 = 2*A**2/2600.-A**3/24000.
      A2 = A**3/2600.-2*A**2/2600.
      LA = LND0
      LB = LAD0
      LC = LAG0/LN0*EF
      SCN = LN*SGRT(-LA**2+4**2)***2*ASIN(LN/4)-2*(R-D/2)*LN
      XAPN = C00-B**3/22+(B**2-LN**2)/3*SGRT(B**2-LN**2)*(LN**2/2.)
      *SGRT(B**2-LN**2)*(LB*B**2/2.)+ASIN(LN/B))-(B-D/2)*LN**2
      CSA = LAC
      XAPA = (LN**2/2.)*LNS0
      XAPP = (XEPAN*XEPA)/(ISPAN*SP2)
      XP12 = XAPAT
      IF(ALPHA.GT.20.) GO TO 20
      XCP = AC00 + A1*X20+A2*XP12
      70 CONTINUE
      RETURN
10 IF(WACH.UY.1.5) GO TO 50
120 CALL LOG10(X0,XOTZ,74,WACH,XCTW,7,LAC,XOTZLA,4,LND,XOTZLN,3,
      *I#*J,XIZ,1)
      GO TO 30
20 IF(WACH.CE.1.) GO TO 40
      APIM = 50.
      GO TO 50
40 APRM = 20.
50 AM = (X2U-XP12)/(XPRM-90.)
      IF(ALPHA.LT.APRM) GO TO 60
      IF(ALPHA.LE.160.) GO TO 60
      X10 = 70.*AM + XP12
      B0 = (-5164000. + 900000.*ALPHA-5200.*ALPHA**2+10.*ALPHA**3)/
      *4000.
      P1 = (4854000.-86400.*ALPHA+310.*ALPHA**2-ALPHA**3)/4000.
      R2 = (-4860000.+86400.*ALPHA-510.*ALPHA**2+ALPHA**3)/4000.
      XCR = B0*AM + P1*(LAD*LND) + 52*X10
      GO TO 70
60 XCP = X20
      GO TO 70
80 XCP = AM*(ALPHA-APRM)+X20
      GO TO 70
90 IF(LAG = 1
      WACH = WACH
      WICH = 1.2
      GO TO 120
100 X01 = X0
      IF(LAG = 0
      JFLAG = 1
      WACH = 1.5
      GO TO 120
110 X02 = X0
      JFLAG = 0
      WACH = WACH
      GO TO 140
      X0 = X02-(X02-X01)*(1.5-WACH)/.3
      GO TO 140

```

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CPT-1

74/74

SUBROUTINE XCPEDC

011000

FAC

115


```

115      RETURN
      80 IFLAG = 0
      JFLAG = 1
      IBT1=IBT
      MACH = 2.0
      GO TO 90
120      JFLAG = 0
      IBT2 = IBT
      MACH = MACHT
      IBT = IBT2-(2.0-MACH)*((IBT2-IBT1)/.7
      RETURN
125      IF (MACH .GE. 2.) GO TO 90
      IFLAG = 1
      MACHT = MACH
      MACH = 1.3
      GO TO 30
130      CALL LOOK1(I1BAS,I1BAS,LAMDA,I1BLM,2,IX,1)
      CALL LOOK1(I1BAS,I1BAS,LAMDA,I1BLM,1,IX,1)
      I1 = I1BAS+1
      CALL LOOK1(I2BAS,I2BAS,LAMDA,I2BLM,1,IX,1)
      CALL LOOK1(I2M,I2M,MACH,I2MACH,2,IX,1)
      CALL LOOK1(I2D8,I2D8,OB,IFD8,2,1,IX,1)
      I2 = I2BAS+I2M+I2D8
      CALL LOOK1(I3AR,I3AR,AR,IFAR,10,IX,1)
      I3 = -5*F3AR
      IF (ALPHA .GT. 90.) GO TO 105
      IBTO = I1-SIN(ALPHA*PI)
      GO TO 110
105      IF (ALPHA .GT. 115.) GO TO 120
      IBTO = I1-(I1-I2)*SIN((ALPHA-90.)/25.)
      GO TO 110
120      IBTO = -19.325*I3+11.926*I2+115.816*I3-8.362*I2)*((ALPHA*PI)
      +((1.46*I2-3.076*I3)*(ALPHA*PI))*.2
110      IBT = IBTO
      IF (JFLAG .EQ. 1) GO TO 100
      RETURN
150      WRITE(6,500)
      500 FORMAT(1X,'MACH NUMBER OUTSIDE ALLOWABLE LIMITS')
      RETURN
      END

```



```

RAD = PI/180.
DP = 0/12.5)
IF(ALPHA.GT.50.) GO TO 10
IF(MACH.GT. 1.) GO TO 20
BETA = SQR(1.-MACH**2)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP1,P,4,PAR,TEAR,5,DE,TDR,4,LAMDA,TLAM,3,IX,IV,
.12.1)
40 A = ALPHA*RAU
DIF = (2.0**3)/(PI/2.0)**3-(3.0**2)/(PI/2.0)**2
XCPBT = XCPC0+DIF*(XCPC0-5)
RETURN
70 IF(MACH.GT. 1.) GO TO 30
BETA = SQR(1.-MACH**2)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP2,P,4,PAR,TEAR,5,DE,TDR,4,LAMDA,TLAM,3,IX,IV,
.12.1)
50 A = (180.-ALPHA)*RAD
DIF = (2.0**3)/(PI/2.0)**3-(3.0**2)/(PI/2.0)**2
XCPBT = XCPC0 + DIF*(XCPC0-5)
RETURN
80 BETA = SQR(MACH**2-1.)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP3,P,4,PAR,TEAR,5,DE,TDR,4,LAMDA,TLAM,3,IX,IV,
.12.1)
GO TO 40
30 BETA = SQR(MACH**2-1.)
PAR = BETAPAR
CALL LOOK3(XCPC0,TCP4,P,4,PAR,TEAR,5,DE,TDR,4,LAMDA,TLAM,3,IX,IV,
.12.1)
GO TO 50
END

```


SUBROUTINE XCPTEH 76/76 OPT=1

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60
GO TO 30
40 CONTINUE
XCPTEU = XCPTEA
XCPTEL = XCPTEU
30 CONTINUE
RETURN
END

014890
014900
014910
014920
014930
014940
014950


```

60      IF(ALPHA-GE. 160.) GO TO 15
        CA = CAO-(CAO-CAPI)*SIN(ALPHAP/57.2957)
        GO TO 40
15      CONTINUE
        CA = CAPI
        GO TO 40
70      IF(ALPHA-GT.90.) GO TO 50
        CAW =(-0.0008 + 0.1501*(MACH/LND) + 0.3641*(MACH/LND)**2 + 0.0928*(MACH/LND)**3
        SMACH/LND)**3 - 0.0409*(MACH/LND)**4 + 0.004*(MACH/LND)**5)/(0.7*
        SMACH**2)
        CALL CSF(RN,MACH,CF)
        CASF = (4.0/5.0)*CFS*WOR
        CAO = CAW + CASF +CDH
        CA = CAO
        GO TO 40
50      IF(ALPHA-GE. 160.) GO TO 60
        CAPI = -(2.9217-9.1867*(MACH)+14.0023*(MACH)**2-8.7943*(MACH)**3+
        12.4985*(MACH)**4-0.2658*(MACH)**5)
        CA = CAO-(CAO-CAPI)*SIN(ALPHAP/57.2957)
        GO TO 40
60      CAPI = -(2.9217-9.1867*(MACH)+14.0023*(MACH)**2-8.7943*(MACH)**3+
        12.4985*(MACH)**4-0.2658*(MACH)**5)
        CA = CAPI
40      CONTINUE
        RETURN
        END

```

```

SUBROUTINE CSF(RN,MACH,CF)
C.....
C THIS PROGRAM CALCULATES THE SKIN FRICTION COEFFICIENT ON THE BODY
C.....
C RN = REYNOLDS NUMBER
C MACH = MACH NUMBER
C CF = SKIN FRICTION COEFFICIENT
C.....
REAL MACH,LAM
G = 1.4
LAM = 1.0/SORT((2.0/((G-1.0)*MACH**2))*1.0)
CF1 = 0.074*((1.0/RN**2))*1.0/((G-1.0)/2.0)*MACH**2)***.44
FCF1 = (ASIN(LAM)/LAM)*1.0/SORT(1.0/((G-1.0)/2.0)*MACH**2))*(-.242/019530
SSORT(CF1))-ALOG10(CF1)*RN)*1.26*(ALOG10(1.0/((G-1.0)/2.0)*MACH**2))
CF2 = CF1 * 0.00001
FCF2 = (ASIN(LAM)/LAM)*1.0/SORT(1.0/((G-1.0)/2.0)*MACH**2))*(-.242/019560
SSORT(CF2))-ALOG10(CF2)*RN)*1.26*(ALOG10(1.0/((G-1.0)/2.0)*MACH**2))
N = 1
10 DCF0DF = ((CF2-CF1)/(FCF2-FCF1))
CF3 = CF2 - DCF0DF*FCF2
IF(FCF2*LT-0.0) GO TO 15
CF3 = CF1 - DCF0DF*FCF1
15 N = N + 1
FCF3 = (ASIN(LAM)/LAM)*1.0/SORT(1.0/((G-1.0)/2.0)*MACH**2))*(-.242/019640
SSORT(CF3))-ALOG10(CF3)*RN)*1.26*(ALOG10(1.0/((G-1.0)/2.0)*MACH**2))
IF(ABS(FCF3)-LE-0.000001) GO TO 20
CF1 = CF2
FCF1 = FCF2
CF2 = CF3
FCF2 = FCF3
IF(M*GT-50.0) GO TO 30
GO TO 10
20 CF = CF3
30 WRITE(6,35)
35 FORMAT(1H0** THE ITERATION HAS GONE THROUGH 50 CYCLES*)
50 CONTINUE
RETURN
END

```

73

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SUBROUTINE LOOK2 74/74 OPT=1

```

C..... SUBROUTINE LOOK2(FT,NR,X,XT,NX,Y,YT,NY,IX,IY,MULT) 018320
C..... TWO-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES) 018330
C..... F=FT(X,Y) 018340
C..... 018350
C..... FUNCTION TABLE FT(NR,NC) 018360
C..... NO. OF ROWS IN FT-TABLE 018370
C..... NC NO. OF COLUMNS IN FT-TABLE 018380
C..... X,Y WORKING VALUES OF INDEPENDENT VARIABLES 018390
C..... XT,YT INDEPENDENT VARIABLE TABLES 018400
C..... NX,NY DIMENSION OF XT,YT-TABLES 018410
C..... *IX,IY X,Y INDEXES ON PREVIOUS LOOKUP (UPDATED ON EACH CALL) 018420
C..... MULT =0, USE PREVIOUS X,Y 018430
C..... =1, LOOKUP NEW X,Y 018440
C..... 018450
C..... DIMENSION FT(1),XT(1),YT(1) 018460
C..... IF(MULT-1)2 018470
C..... 1 CALL INDEX(YT,NY,IY,KEEP,RY) 018480
C..... I = 1+(IY-1)*NR 018490
C..... II = 1+NR 018500
C..... 2 CALL LOOK1(F,FT(1),X,XT,NX,IX,MULT) 018510
C..... IF(KEEP-1)3,4,3 018520
C..... 3 CALL LOOK1(F2,FT(1),X,XT,NX,IX,1) 018530
C..... F=(F2-F)*RY+F 018540
C..... 4 RETURN 018550
C..... END 018560

```

```

SUBROUTINE INDEX(X,XI,NX,IH,KEEP,RATIO)
C.....018010
C TABLE INDEX LOOKUP ROUTINE (O = RETURNED VALUES) 018030
C X WORKING VALUE OF INDEPENDENT VARIABLE 018040
C XI INDEPENDENT VARIABLE TABLE XT(NX) 018050
C NX DIMENSION ON X-TABLE 018060
C IH INDEX OF PREVIOUS LOOKUP (UPDATED EACH CALL) 018070
C *KEEP = 0 X-NEXT ANY AT. INTERPOLATION WAS REQUIRED. 018080
C      = 1 X-FO.AT(IH). INTERPOLATION NOT REQUIRED. 018090
C *RATIO INTERPOLATION RATIO 018100
C.....018110
C DIMENSION XT(1) 018120
C RATIO = 0. 018130
C KEEP = 0 018140
1 IF(NX-IH).EQ.1,2 018150
1 IX = NX-1 018160
2 IF(IX-1).GE.3,4 018170
3 IX = 1 018180
4 IF(NX-1).GT.10,5 018190
5 IF(NT(IH)-NX).GT.10,7 018200
6 IF(NT(IH+1)-X).GT.9,11 018210
7 IX = IH-1 018220
8 IF(IX-1).GE.5 018230
9 IX = IX+1 018240
10 IF(IX-NX).GT.10,10 018250
9 IX = IX+1 018260
10 KEEP = 1 018270
RETURN 018280
11 RATIO = (X-XT(IH))/(XT(IH+1)-XT(IH)) 018290
END 018300
018310

```


Appendix B. DESCRIPTION OF SUBROUTINES AND PROGRAM LISTING

Table B-1 lists the subroutines and gives their basic function.

A detailed description of each subroutine will not be included in this report. The logic and procedures required of each included method are discussed in detail in Reference 1. The applicable section of Reference 1 for each of the Methodology Program Subroutines is listed in Table B-1.

TABLE B-1. LIST OF PROGRAM ELEMENTS

SUBPROGRAM NAME	REF. 1 SECTION	FUNCTION OF SUBPROGRAM
MAIN		Controls input and output to the program. Uses various subroutines to calculate aerodynamic coefficients and centers of pressure for total missile and isolated components.
CNTPHI	SEC.5.2.1	Calculates tail normal force coefficient in presence of a cylindrical body as a function of roll angle. (Angle of attack limited to 0 to 45 degrees).
CNTT	SEC.5.1.4	Calculates tail normal force coefficient of an isolated tail (angle of attack 0 to 180 degrees).
BRIT		Contains data required by several other Methodology subroutines. Data is taken from British Data Sheets. (Reference 3).
CNBOD	SEC.5.1.1	Calculates body alone normal force coefficient (angle of attack 0 to 180 degrees).
XCPBOD	SEC.5.1.2	Calculates body alone center of pressure measured in calibers from the nose. (Angle of attack 0 to 180 degrees).
IBTT	SEC.5.2.4	Calculates body normal carry over force coefficient.
XCPBTT	SEC.5.2.5	Calculates tail-to-body carry over normal force center of pressure.
XCPTBB	SEC.5.2.2	Calculates the tail chordwise center of pressure (upper and lower bound)/ tail root chord, measured aft from root chord leading edge.

SUBPROGRAM NAME	REF. 1 SECTION	FUNCTION OF SUBPROGRAM
YCPTS	SEC.5.2.3	Calculates tail spanwise center of pressure for isolated tail.
XCPTT	SEC.5.1.5	Calculates chordwise center of pressure for isolated tail for roll angle = 0.
PHCC		Required by several other Methodology Subroutines.
AXIAL	SEC.5.1.3	Calculates the axial force coefficient for the missile body.
CSF	SEC.5.1.3	Calculates the skin friction coefficient for the missile body.
LOOK1		One-dimensional table look-up subroutine.
LOOK2		Two-dimensional table look-up subroutine.
LOOK3		Three-dimensional table look-up subroutine.
INDEX		Required for subroutines LOOK1, LOOK2, and LOOK3.

A complete program listing follows.

REFERENCES

1. Aiello, G.F., "Aerodynamic Methodology (Bodies With Arbitrary Roll Angles, Transonic and Supersonic)", Final report on USAMICOM Contract DAAH01-74-C-0621, OR 14,145, April 1976.
2. Spring, D.J., Derrick, J.N., and Winn, G.C., "An Assessment of the Martin-Marietta High Angle of Attack Aerodynamic Methodology for Body-Tail Missiles", TR RD-76-33, US Army Missile Command, June 1976.
3. Royal Aeronautical Society, Data Sheets, Wings 5.01.03.03, 5.01.03.04, 5.01.03.05, and 5.01.03.06.

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